

Progressing G.fast

contributions from 4GBB consortium to standards

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Chenguang Lu – Ericsson



1. Progressing G.fast – how did it originate?

MUSE Consortium

	2006	2007	2008	2009	2010	2011	2012	2013	2014	2015	
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1. Progressing G.fast – how did it originate?

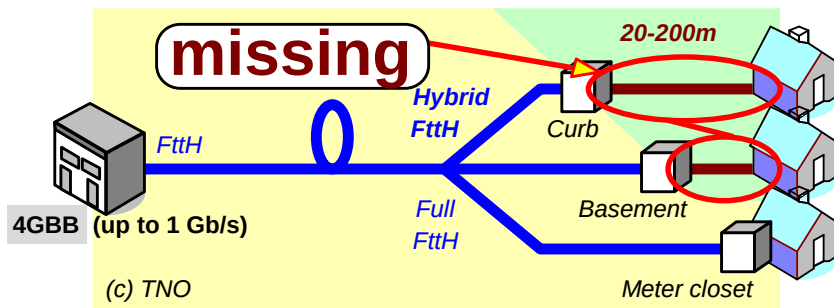
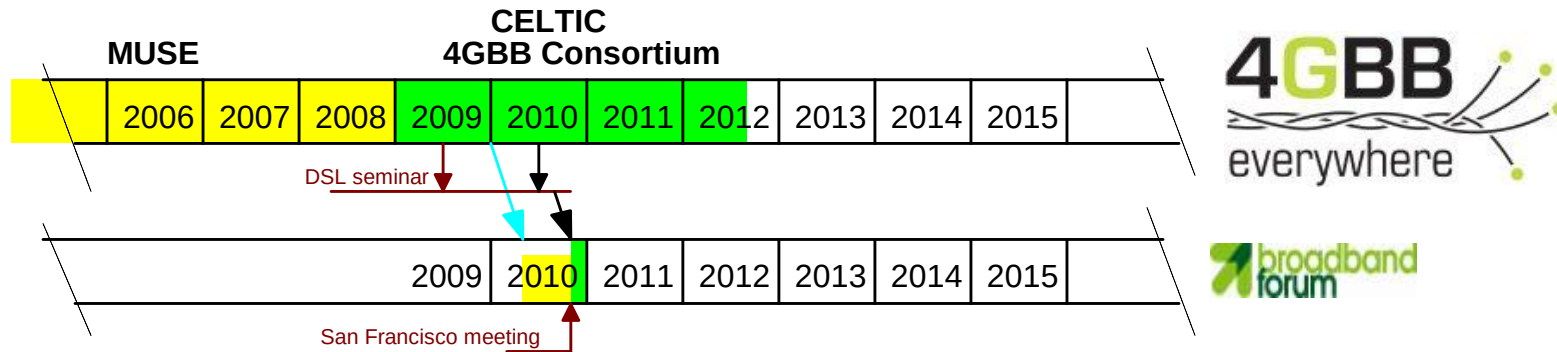


Aims:

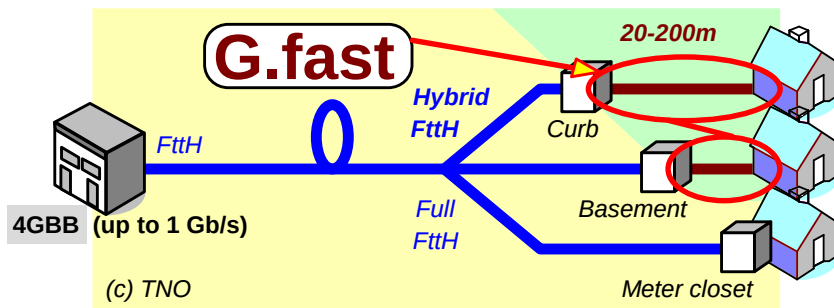
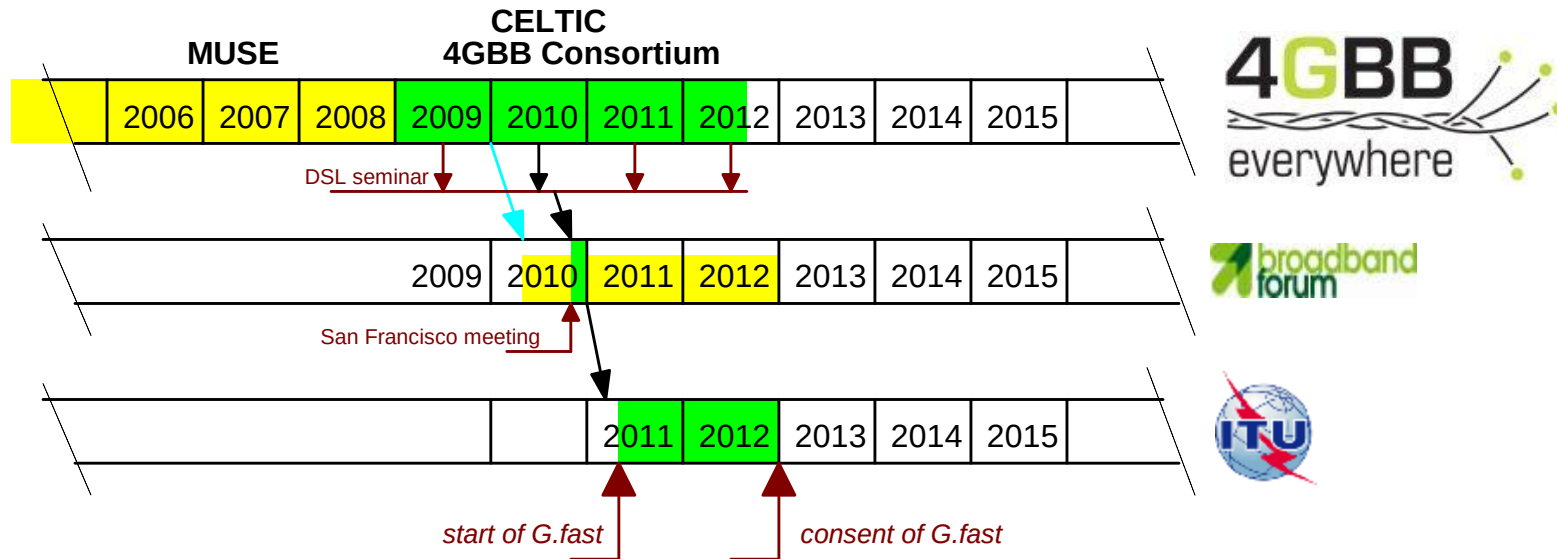
- show feasibility
- initiate a standard
- bring the industry into motion



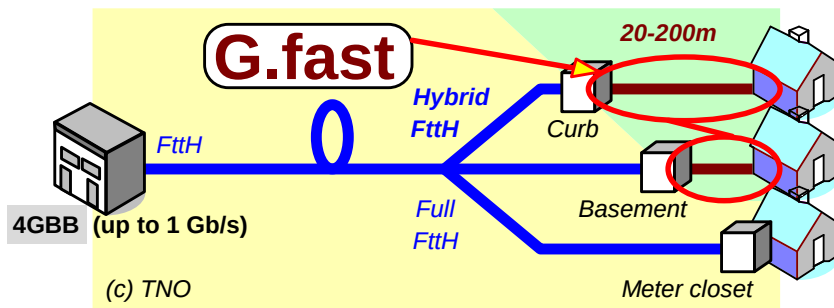
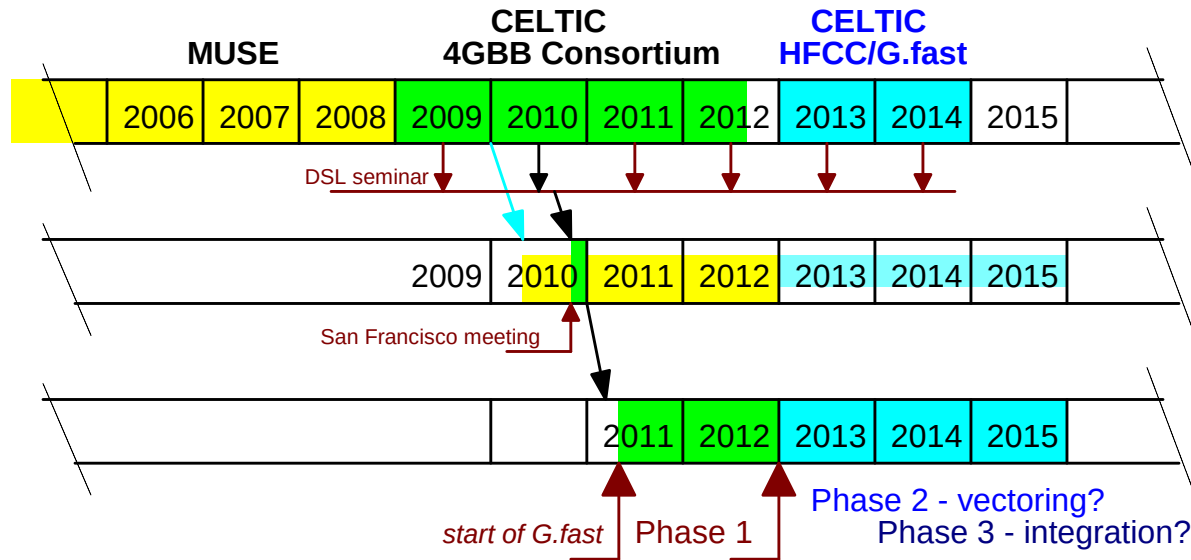
1. Progressing G.fast – how did it originate?



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1. Progressing G.fast – how will it continue?



1. Progressing G.fast – on what topics?

e.g. by developing knowledge on cable modelling & simulations

- Chapter 1 – Progressing G.fast
- Chapter 2 – Progress on cable transmission modeling
- Chapter 3 – Progress on crosstalk modeling
- Chapter 4 – Progress on performance studies

1. Progressing G.fast – on what topics?

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- Chapter 4 – Progress on performance studies

Bitrate targets for G.fast, as agreed within ITU

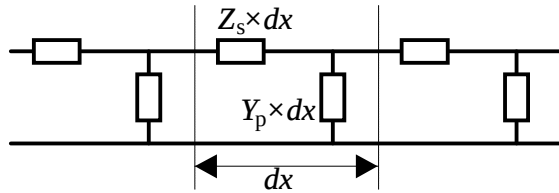
aimed service rates (US+DS rates) under noisy conditions from 8 disturbers

note: different service rate definitions are under discussion

- agreed: at least 10Mb/s when deployed on loops with exceptional length and noise
- agreed: 150 Mb/s @ 250m
- agreed: 200 Mb/s @ 200m
- agreed: **500 Mb/s** @ 100m (typically a FTTB deployment) à *2×500 Mb/s with bonding*
- agreed: **500 Mb/s** @ 50m when **above 17.7MHz**, and not too bad noise
- agreed: **up to 1Gb/s** on shorter loops (protocol should not prevent 1Gb/s)



2. Progress on cable transmission modeling



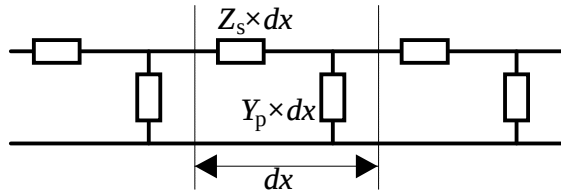
$$R_s(j\omega) = \text{real}(Z_s(j\omega))$$

$$G_p(j\omega) = \text{real}(Y_p(j\omega))$$

$$L_s(j\omega) = \text{imag}(Z_s(j\omega))/w$$

$$C_p(j\omega) = \text{imag}(Y_p(j\omega))/w$$

2. Progress on cable transmission modeling

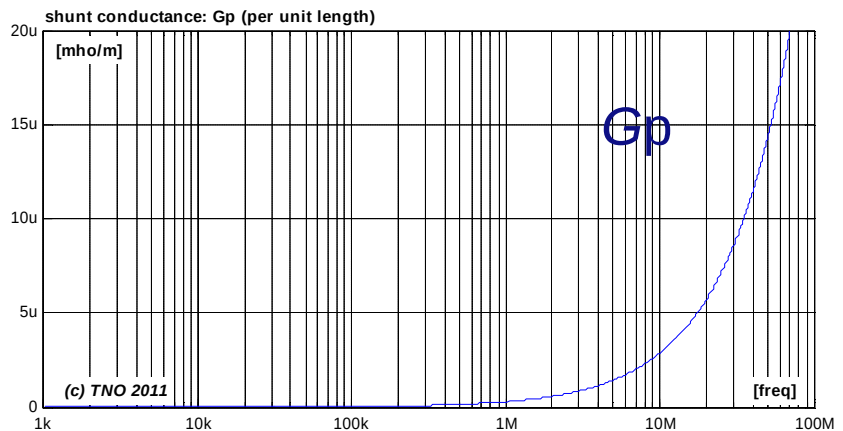
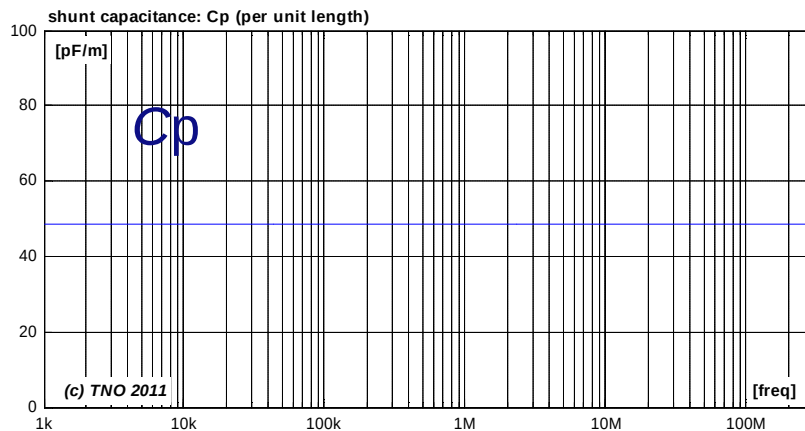
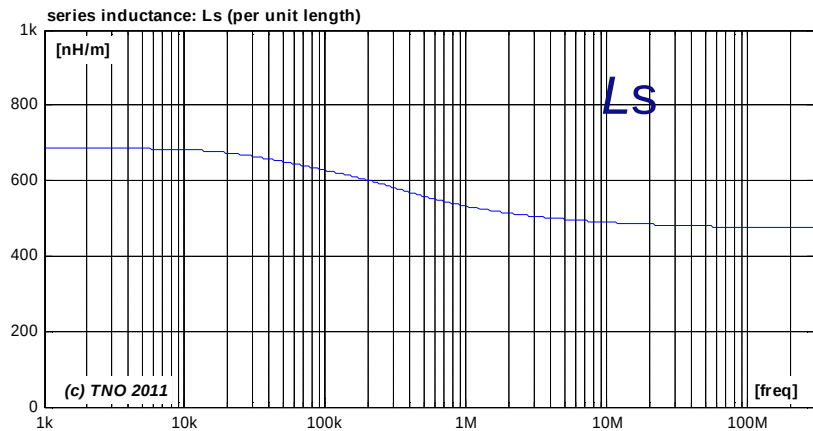
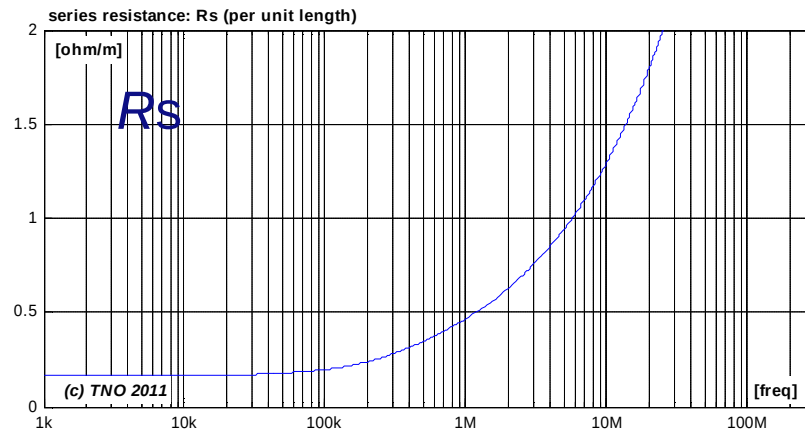


$$R_s(j\omega) = \text{real}(Z_s(j\omega))$$

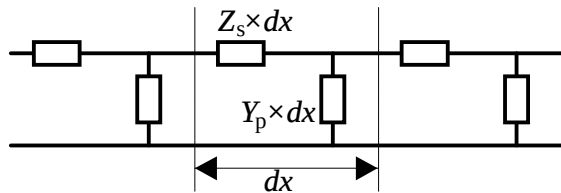
$$G_p(j\omega) = \text{real}(Y_p(j\omega))$$

$$L_s(j\omega) = \text{imag}(Z_s(j\omega))/\omega$$

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2. Progress on cable transmission modeling

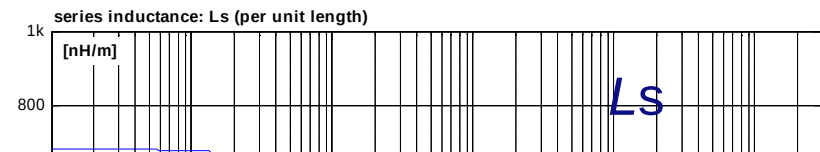
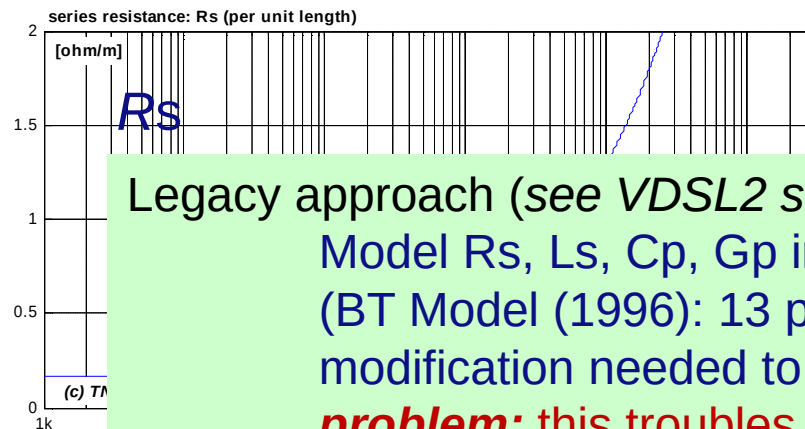


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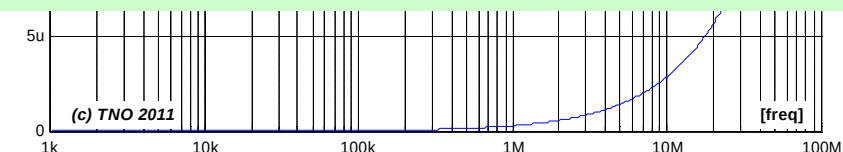
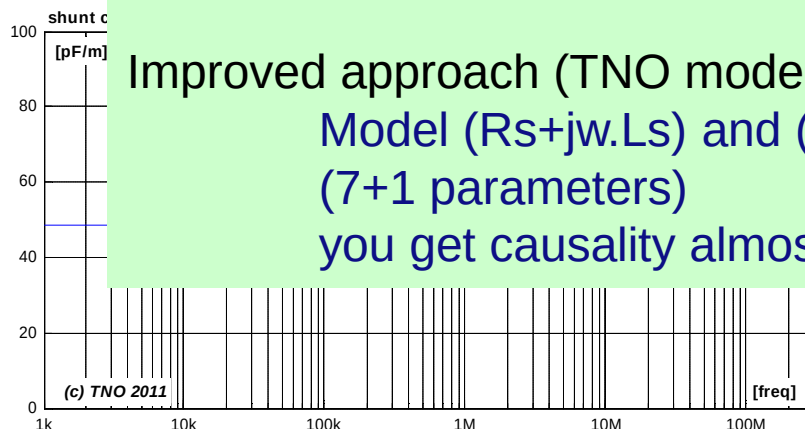
Legacy approach (see *VDSL2 standard*)

Model R_s , L_s , C_p , G_p independently, using 4 functions of “ ω ”
(BT Model (1996): 13 parameters, KPN Model (1997), etc)
modification needed to make impulse response **causal**

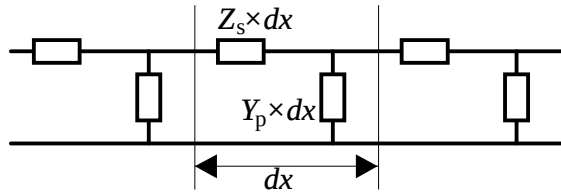
problem: this troubles time-domain simulations

Improved approach (TNO model, 2009/2011):

Model $(R_s + j\omega L_s)$ and $(G_p + j\omega C_p)$, using 2 functions of “ $j\omega$ ”
(7+1 parameters)
you get causality almost for “free” (*if done in a clever way*)



2. Progress on cable transmission modeling

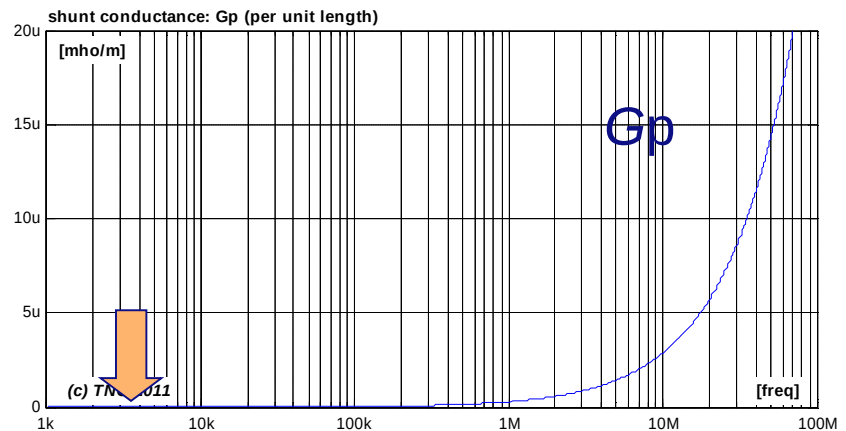
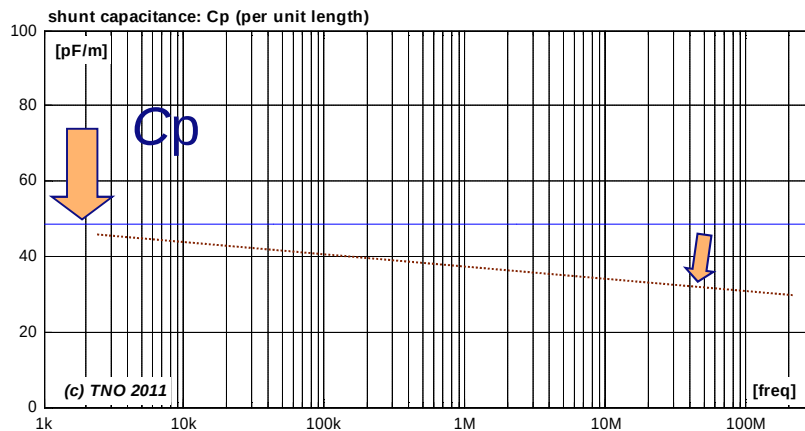
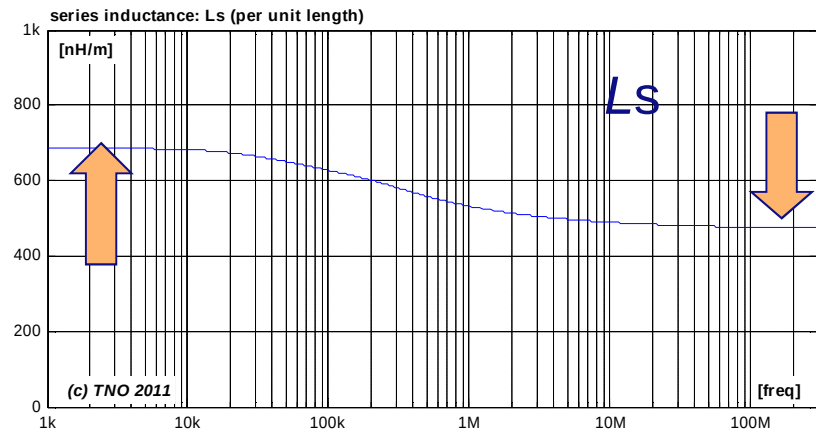
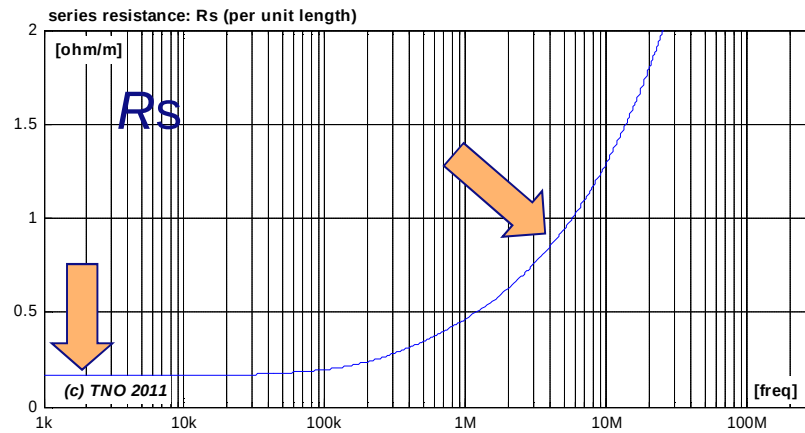


$$R_s(j\omega) = \text{real}(Z_s(j\omega))$$

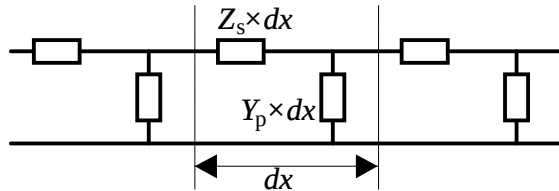
$$G_p(j\omega) = \text{real}(Y_p(j\omega))$$

$$L_s(j\omega) = \text{imag}(Z_s(j\omega))/\omega$$

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2. Progress on cable transmission modeling - expressions for impedance Z_s

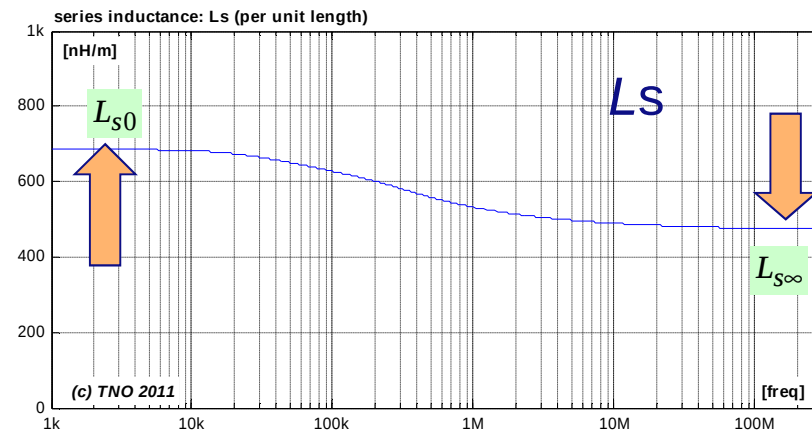
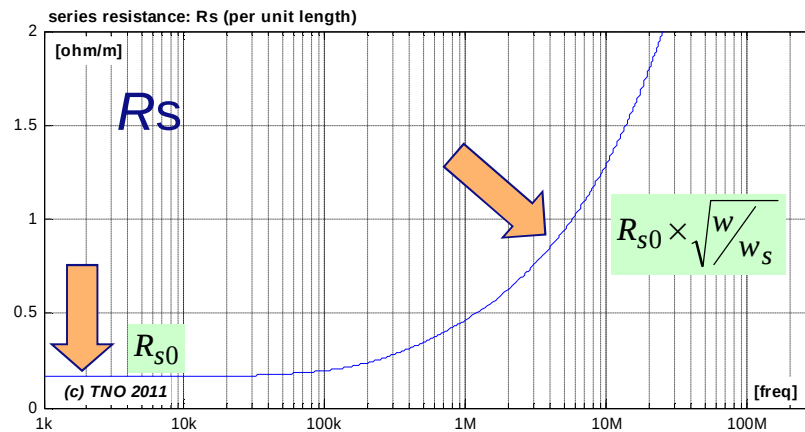


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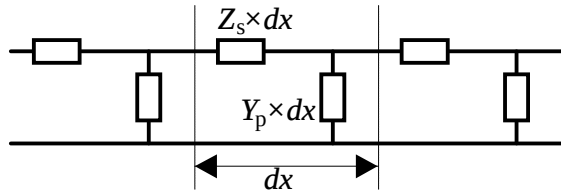
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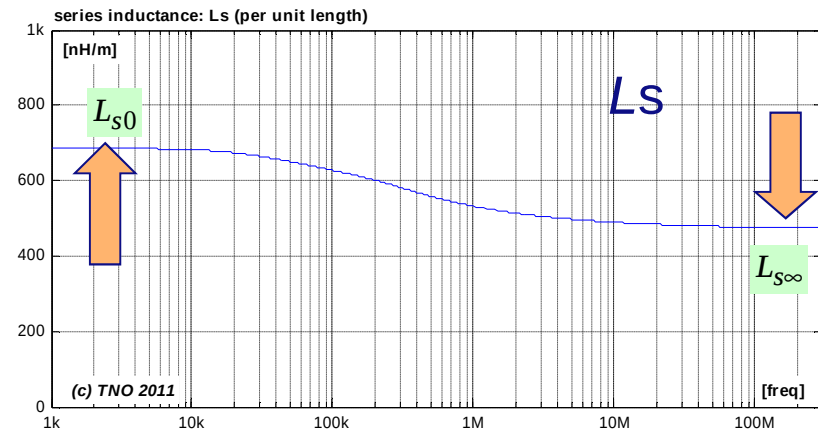
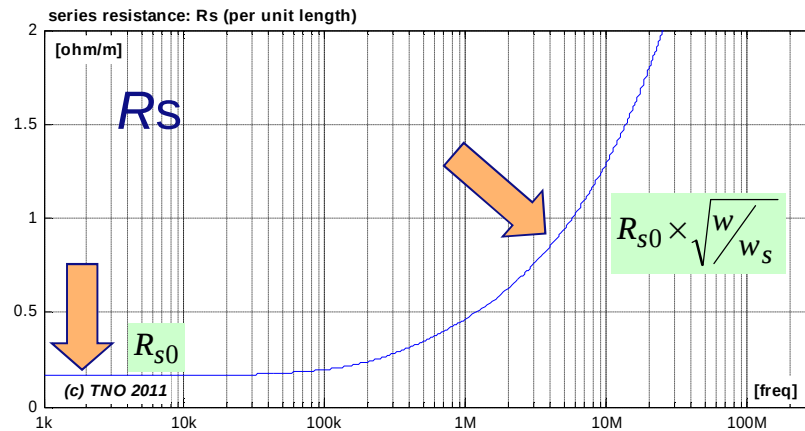


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Approach: take observations as parameters

$$L_{s\infty}, R_{s0}, w_s, q_s$$

parameters

$$L_{s0} = L_{s\infty} + (R_{s0}/w_s)/q_s$$

substitution

$$Q_Z(j\Omega)$$

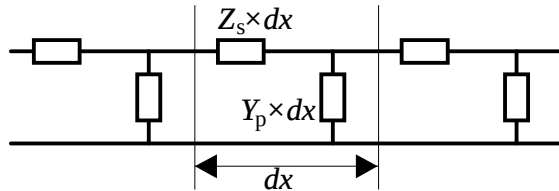
glue (shaping function)



$$Z_s(j\omega) = j\omega \cdot L_{s\infty} + R_{s0} \times \left(1 - q_s + q_s \cdot Q_Z \left(\frac{j\omega}{q_s^2 \cdot w_s} \right) \right)$$

Q_Z is restricted by certain analytical properties

2. Progress on cable transmission modeling - expressions for impedance Z_s

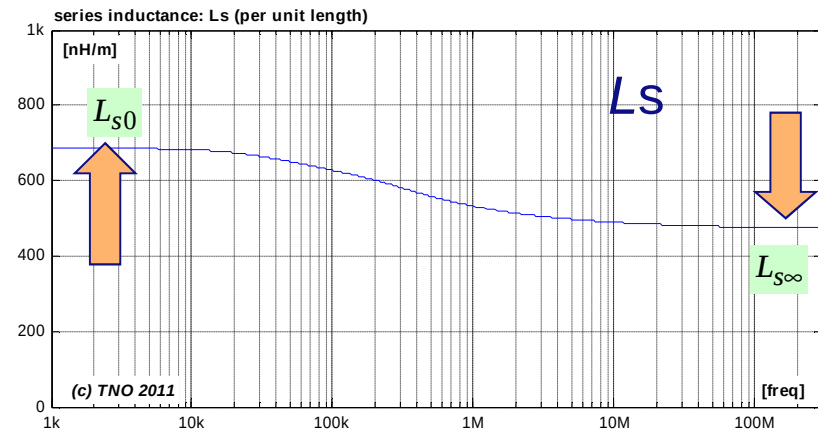
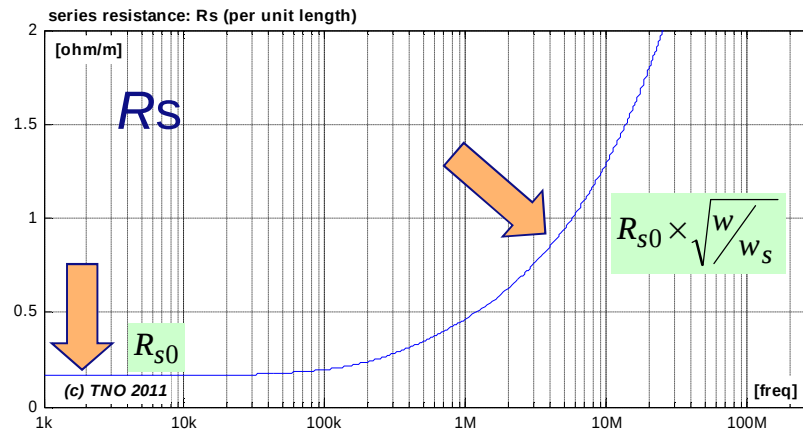


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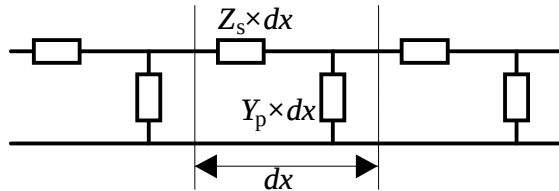
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Q_Z is restricted by certain analytical properties

The simplest form of Q_Z is already very good

$$Z_s(j\omega) = j\omega \cdot L_{s\infty} + R_{s0} \times \left(1 - q_s + \text{sqrt} \left(q_s^2 + 2 \cdot \frac{j\omega}{w_s} \right) \right)$$

2. Progress on cable transmission modeling - expressions for admittance Y_p

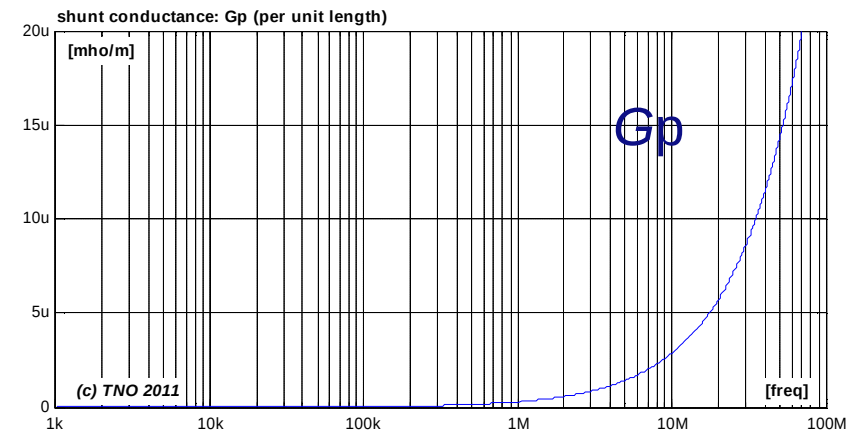
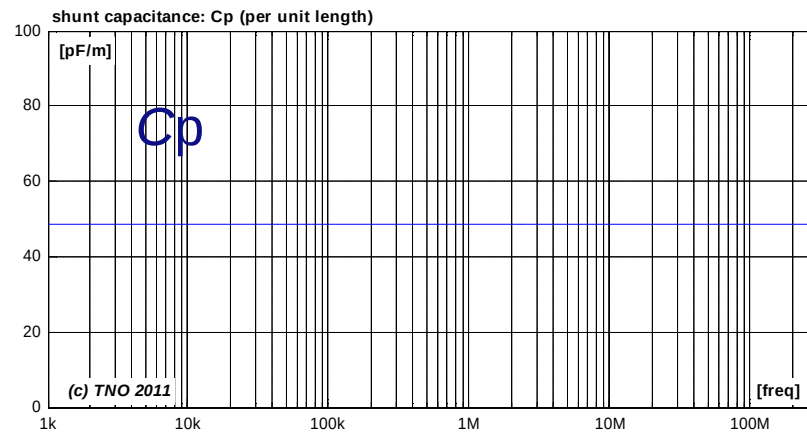


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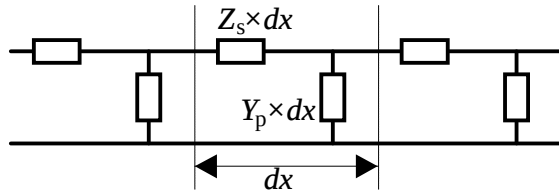
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2. Progress on cable transmission modeling - expressions for admittance Y_p

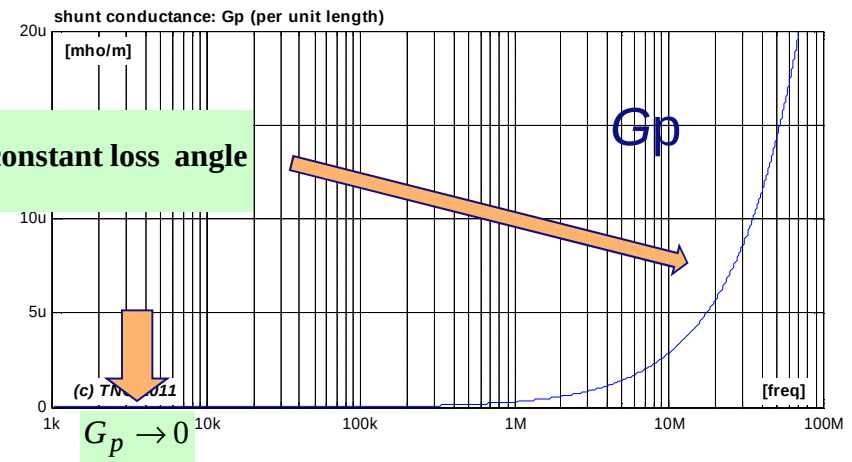
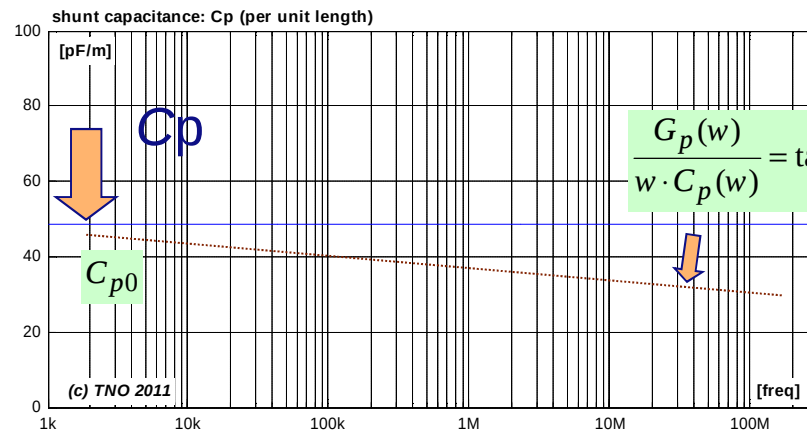


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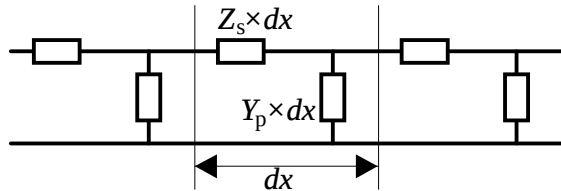
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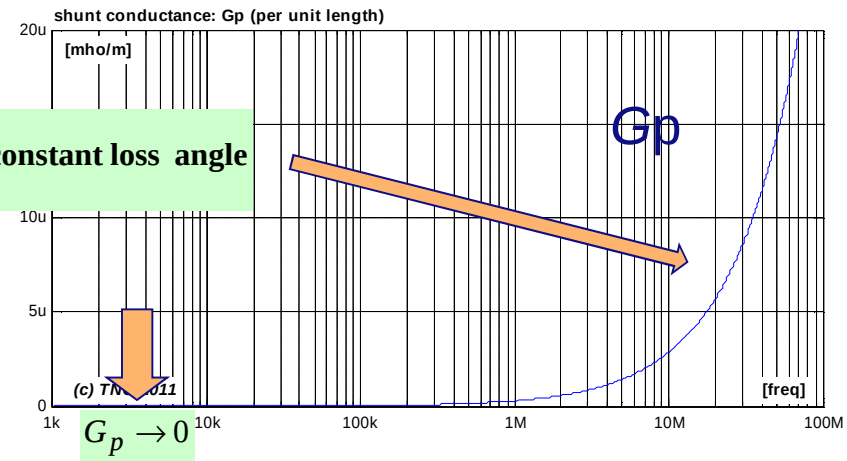
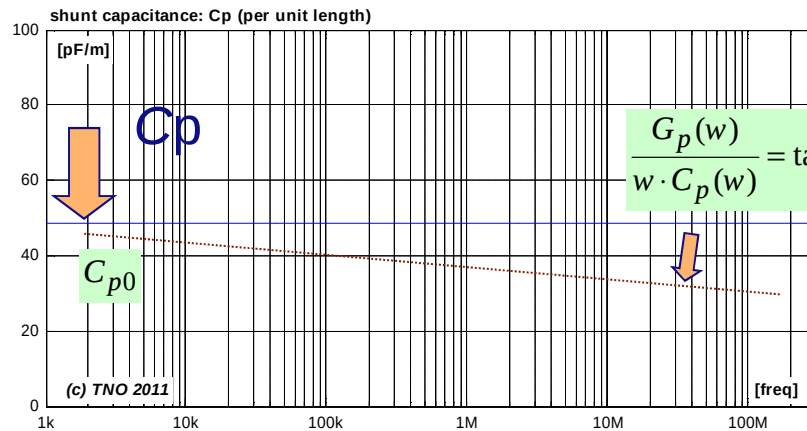


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Approach: take observations as parameters

C_{p0}, f, w_d parameters

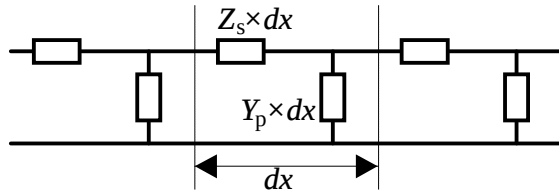
$Q_Y(j\omega)$ glue (shaping function)



$$Y_p(j\omega) = j\omega \cdot C_{p0} \times \left[Q_Y\left(\frac{j\omega}{w_d}\right) \right]^f$$

Q_Y is restricted by certain analytical properties

2. Progress on cable transmission modeling - expressions for admittance Y_p

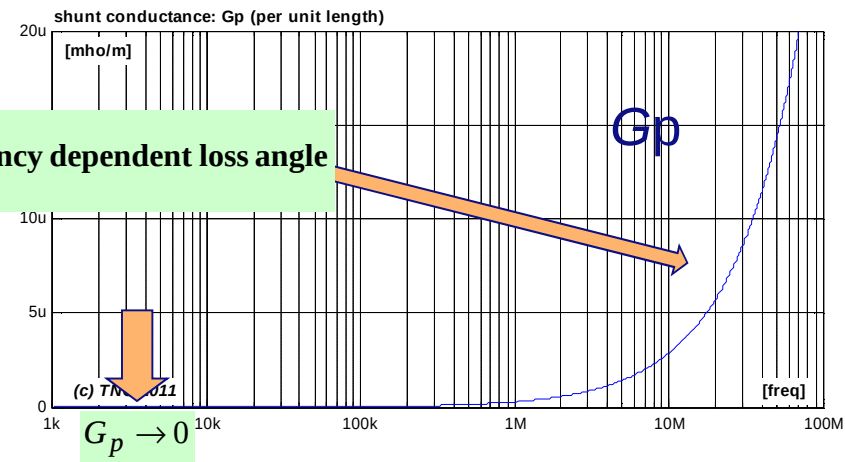
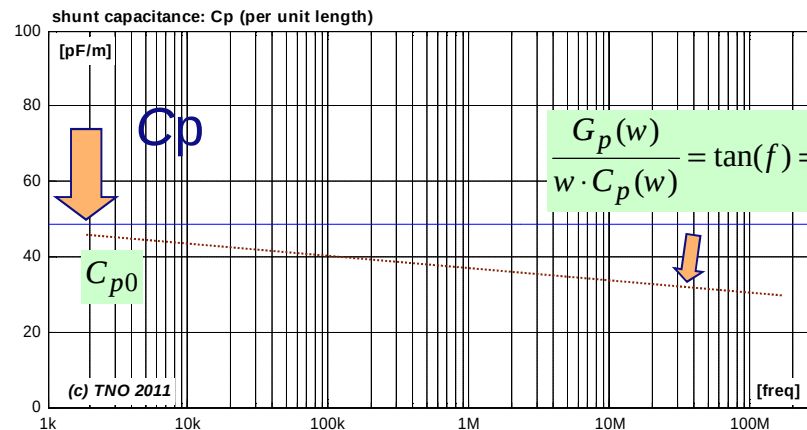


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Approach: take observations as parameters

C_{p0}, f, q_c, w_d parameters

$Q_Y(j\omega)$ glue (shaping function)



$$Y_p(j\omega) = j\omega \cdot C_{p0} \times \left[Q_Y\left(\frac{j\omega}{w_d}\right) \right]^f \times (1 - q_c) + j\omega \cdot C_{p0} \times q_c$$

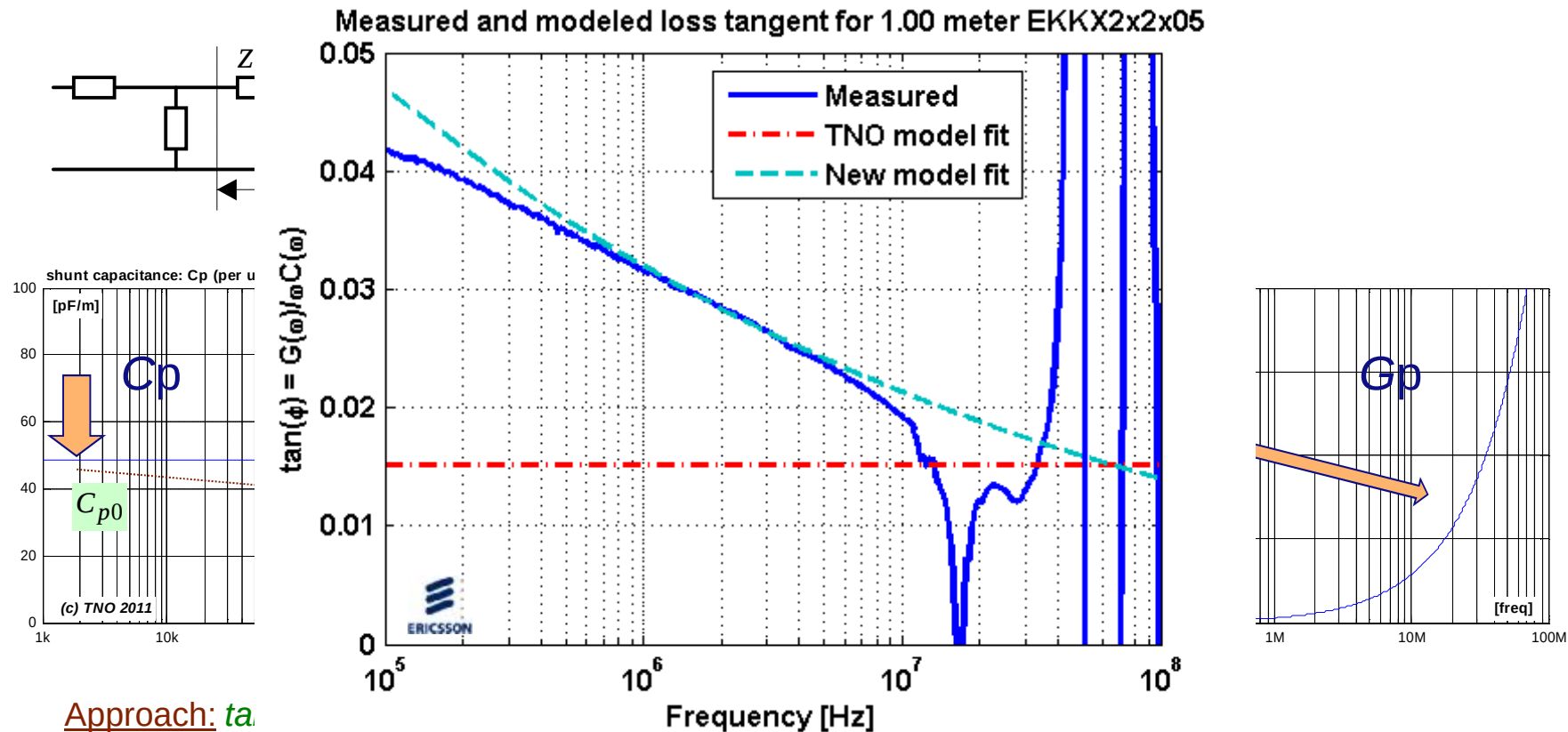
Q_Y is restricted by certain analytical properties

**Refinement from Ericsson+LTH
contributed to last ITU meeting**



Relevant when dielectric loss becomes significant

2. Progress on cable transmission modeling - expressions for admittance Y_p



Approach: *ta*

C_{p0}, f, q_c, w_d parameters

$Q_Y(jw)$ glue (shaping function)



$$Y_p(jw) = jw \cdot C_{p0} \times \left[Q_Y \left(\frac{jw}{w_d} \right) \right]^f \times (1 - q_c) + jw \cdot C_{p0} \times q_c$$

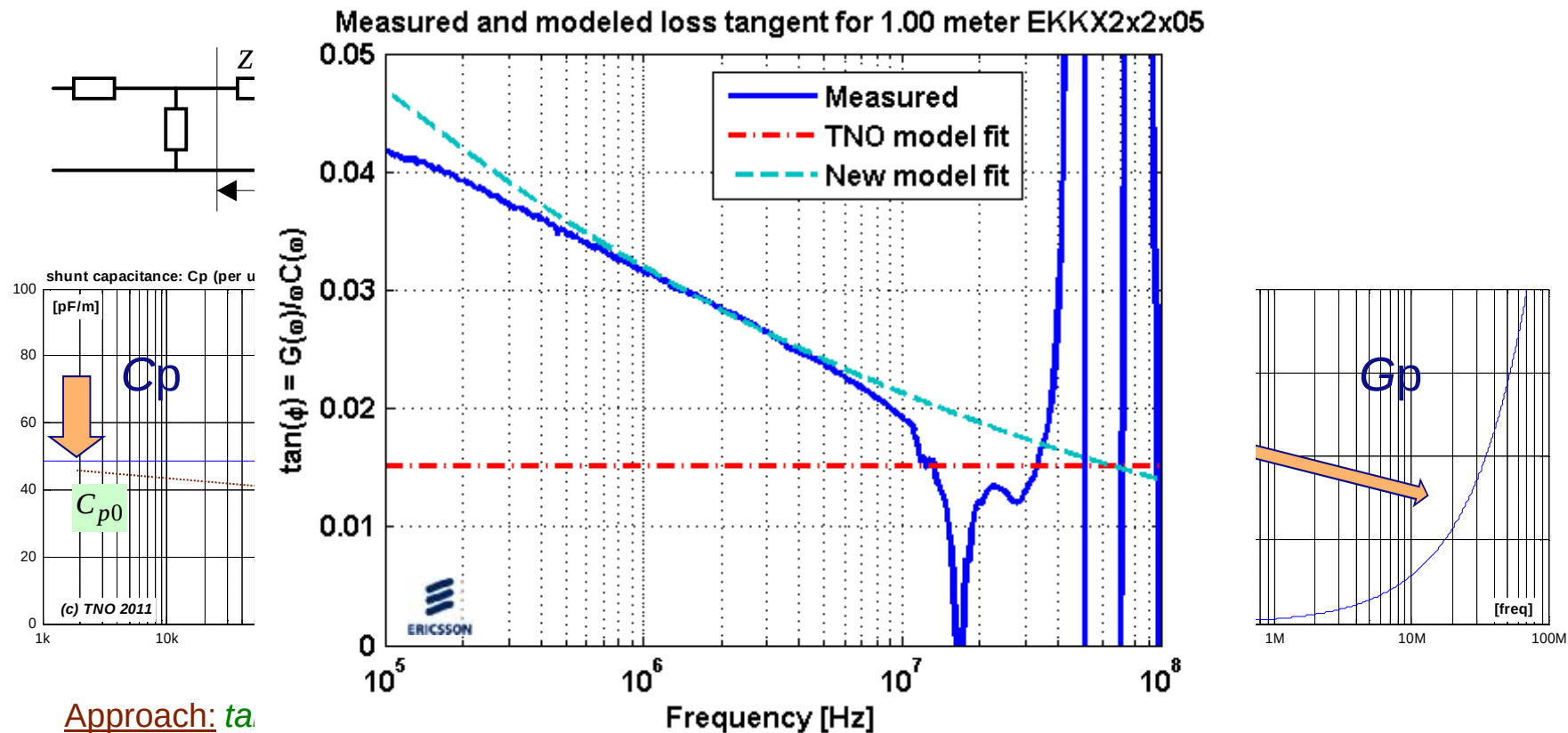
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Q_Y is restricted by certain analytical properties

The simplest form of Q_Y is already very good

$$Y_p(j\omega) = j\omega \cdot C_{p0} \times \left(1 + \frac{j\omega}{w_d} \right)^{-2 \cdot f / p} \times (1 - q_c) + j\omega \cdot C_{p0} \times q_c$$

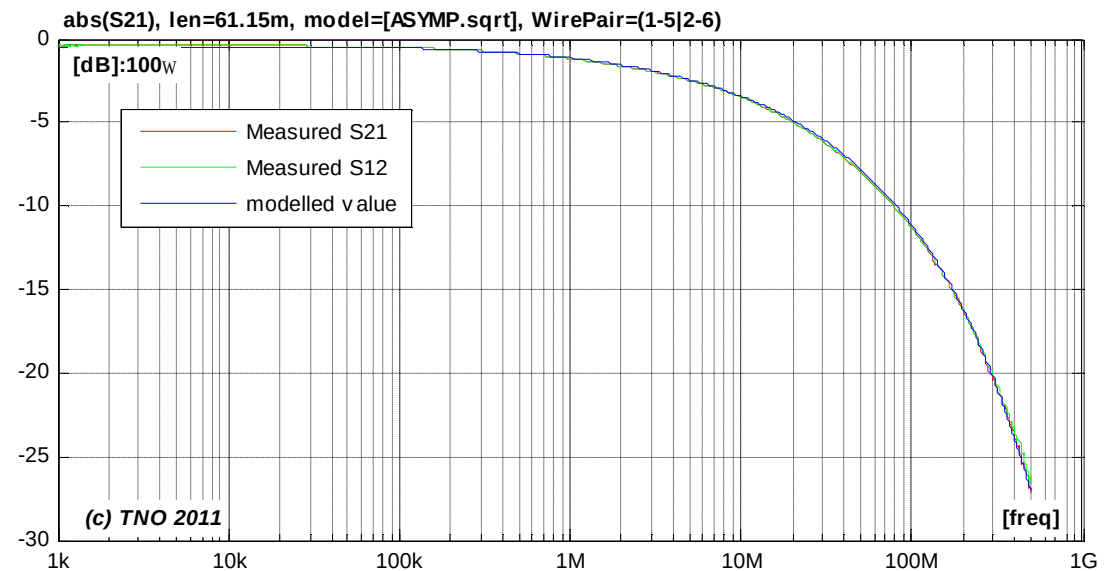
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2. Progress on cable transmission modeling - results

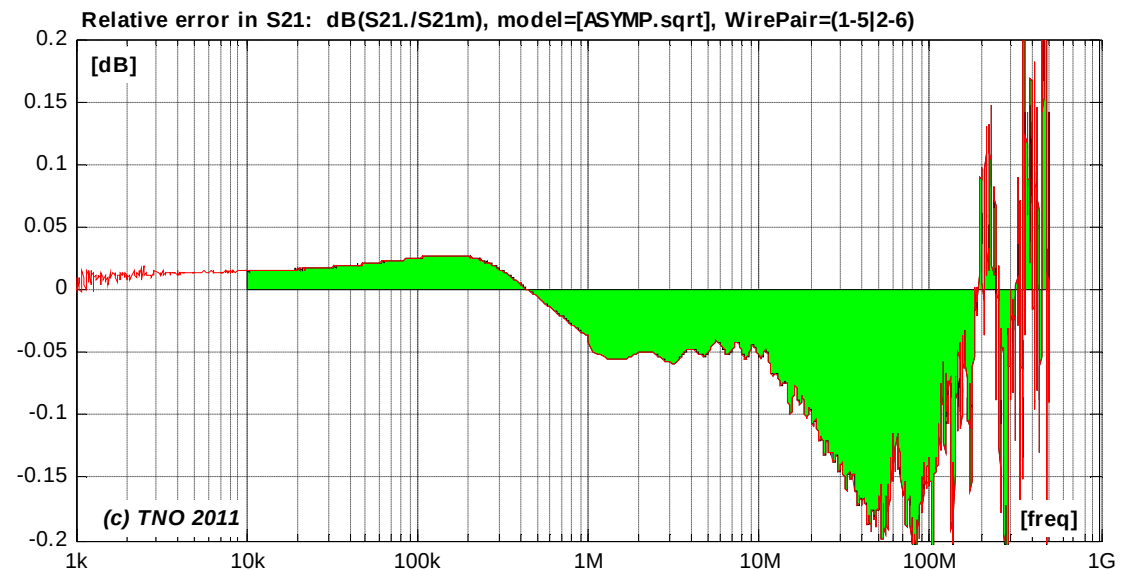
CAT5e cabling



61m



232m



2. Progress on cable transmission modeling - results

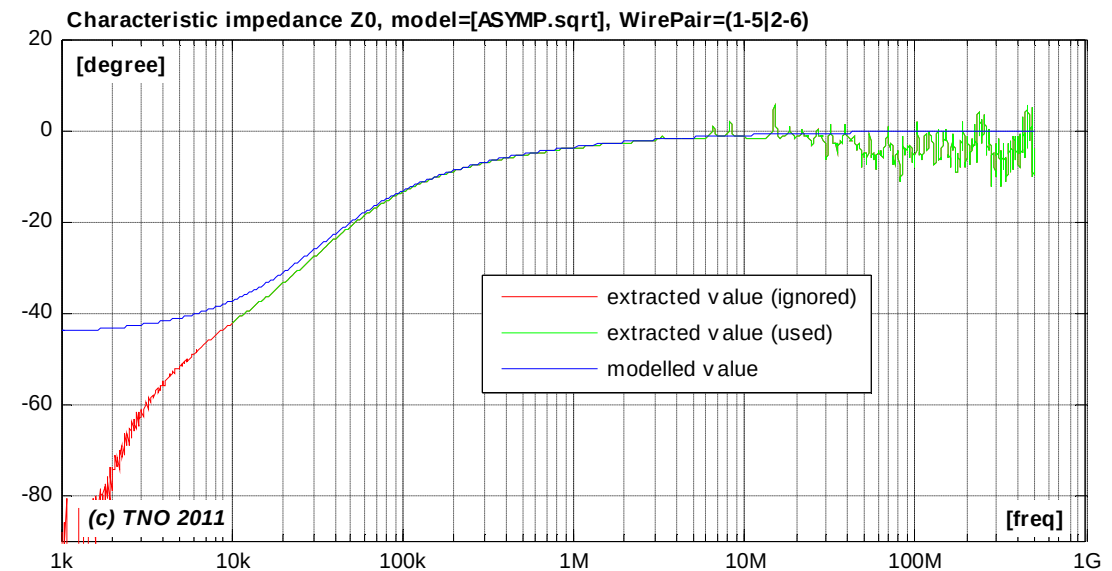
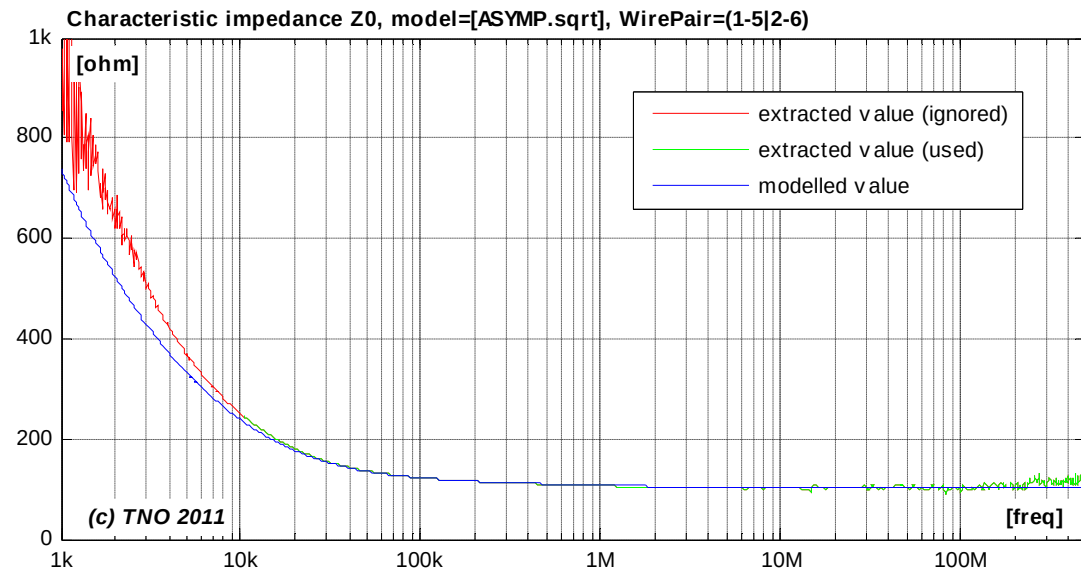
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2. Progress on cable transmission modeling - results

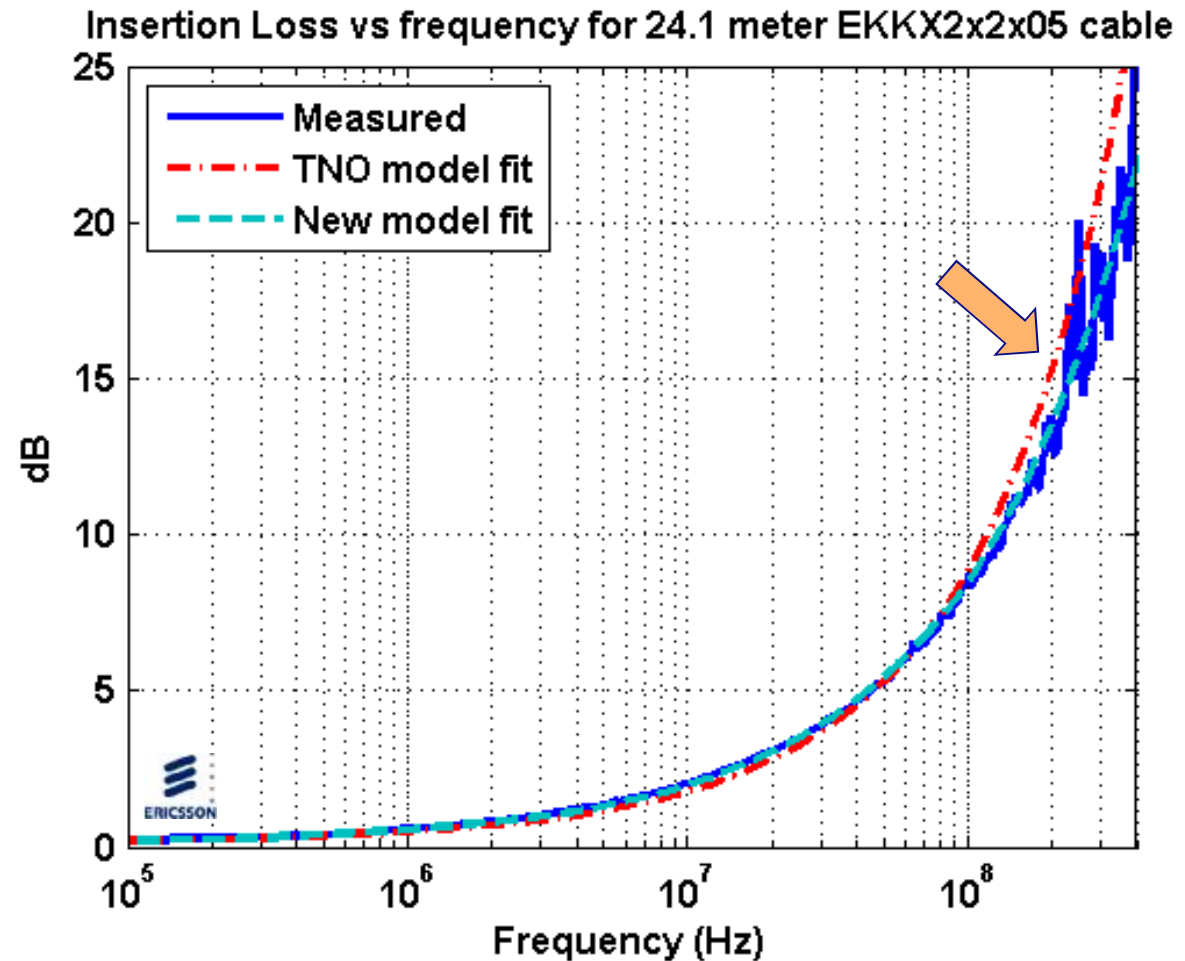
PVC insulated drop cable

Dielectric losses become significant;

Use of proposed refinement from Ericsson and LTH offer valuable improvements



24m

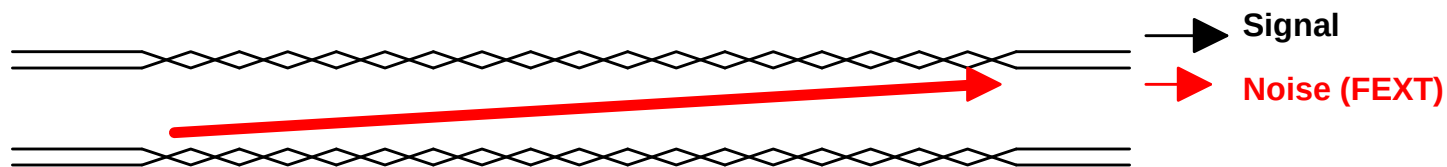


2. Progress on cable transmission modeling - results

New approach

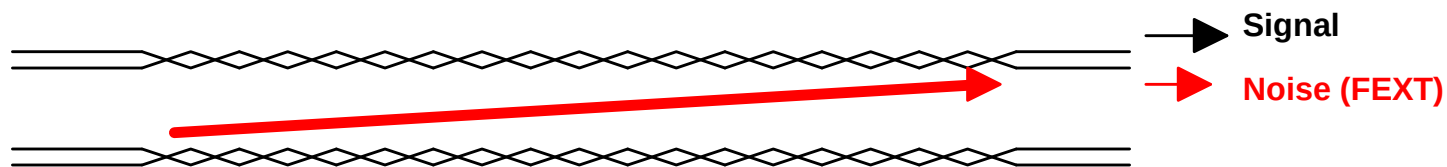
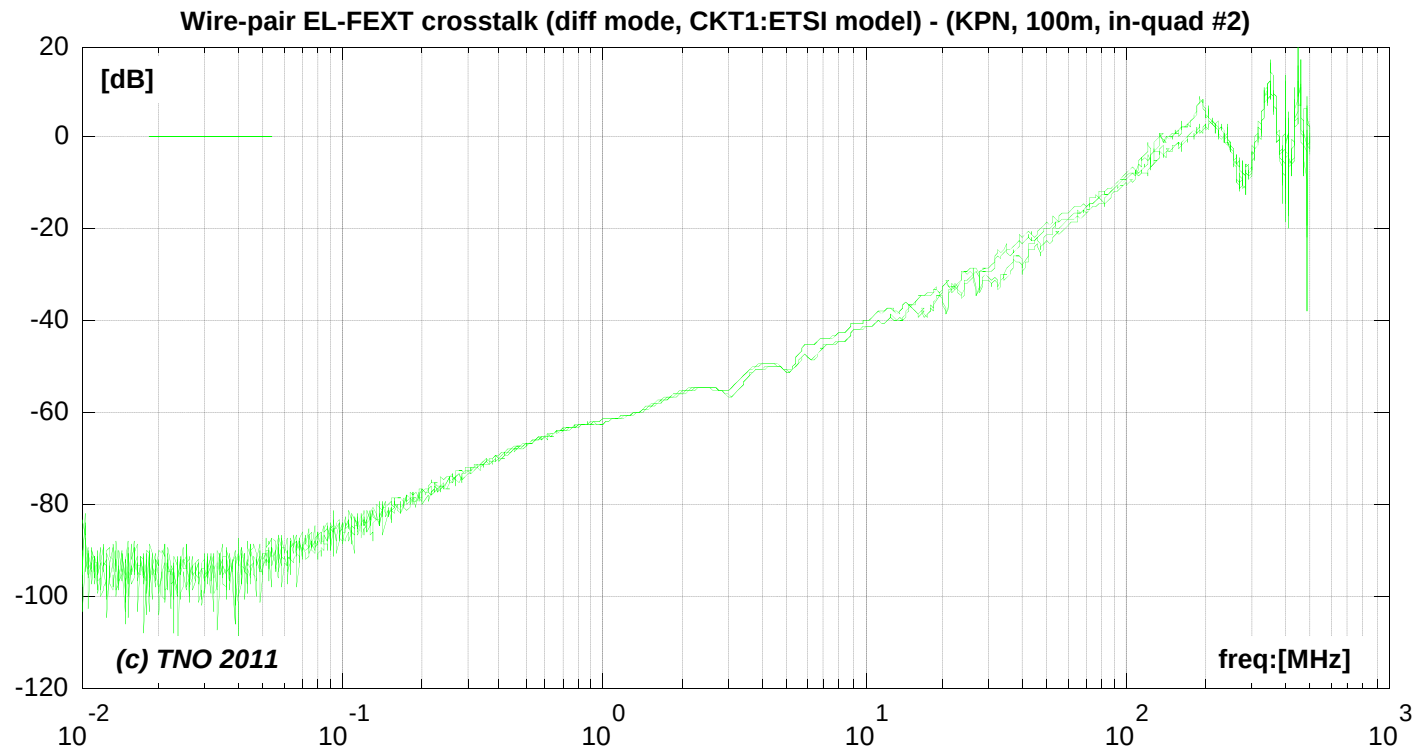
has gained acceptance in ITU

3. Progress on crosstalk modeling - EL-FEXT, legacy approach



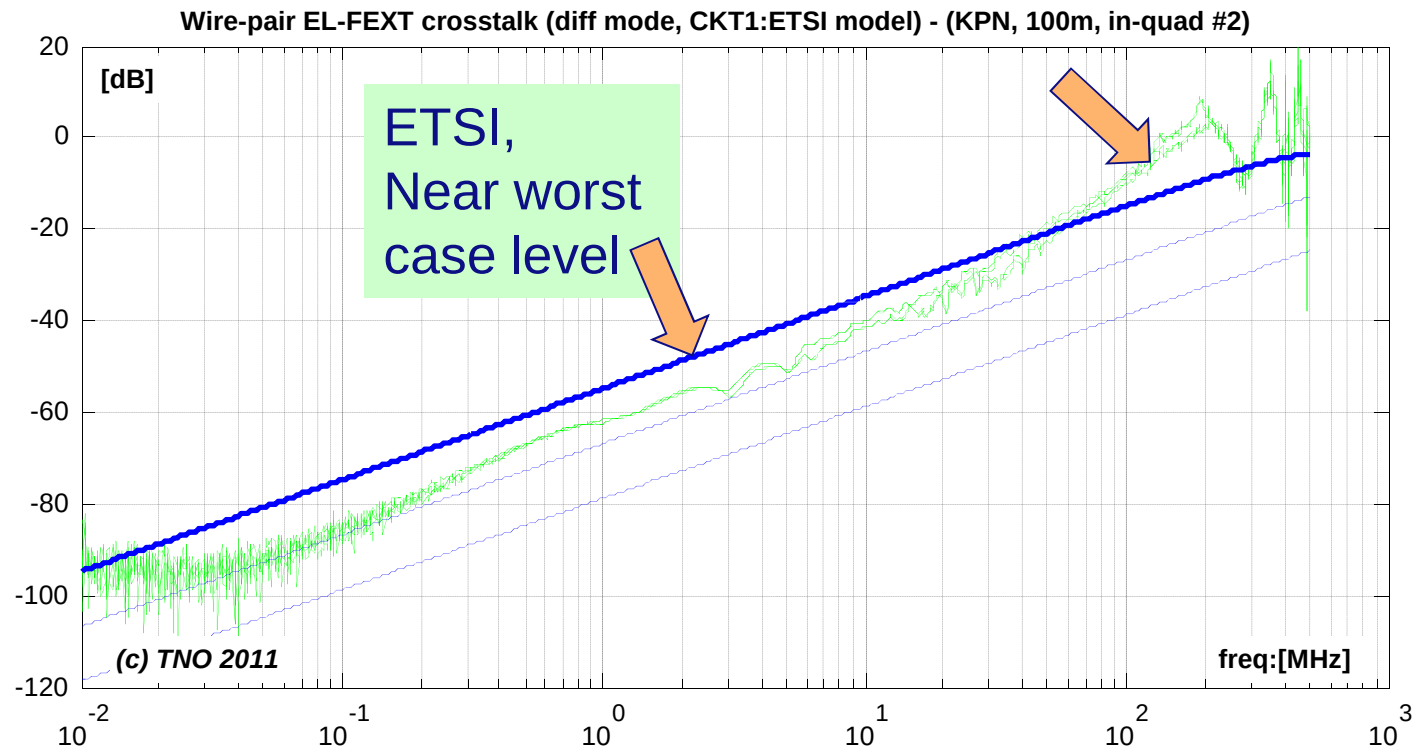
$$\text{EL - FEXT} = \frac{\text{Noise (FEXT)}}{\text{Signal}} = \frac{1}{\text{S/N ratio}}$$

3. Progress on crosstalk modeling - EL-FEXT, legacy approach



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3. Progress on crosstalk modeling - EL-FEXT, legacy approach



Legacy model: (FSAN)
EL-FEXT is linear proportional
with the frequency.

Too low for higher frequencies

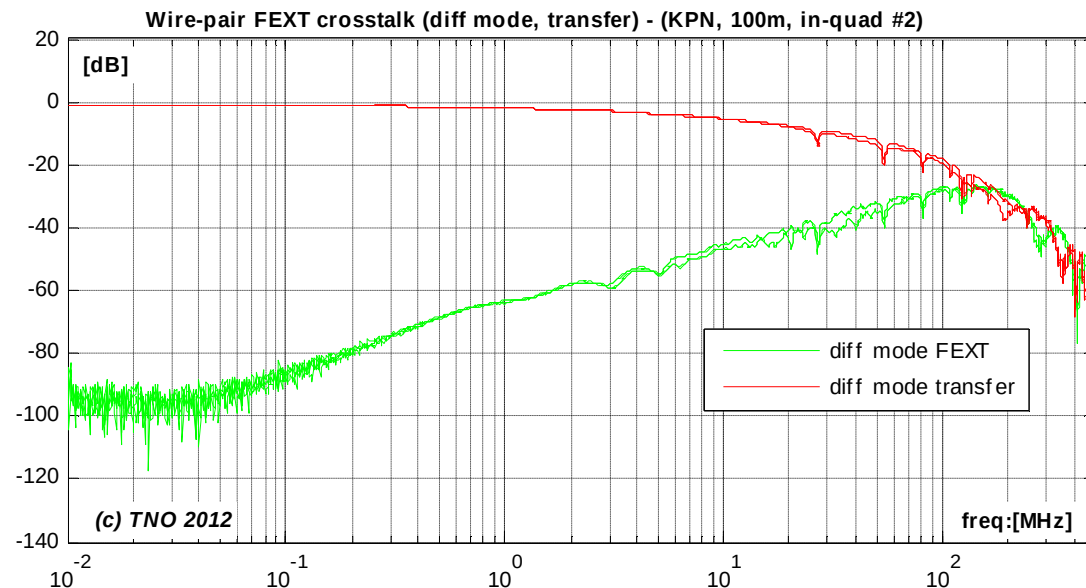
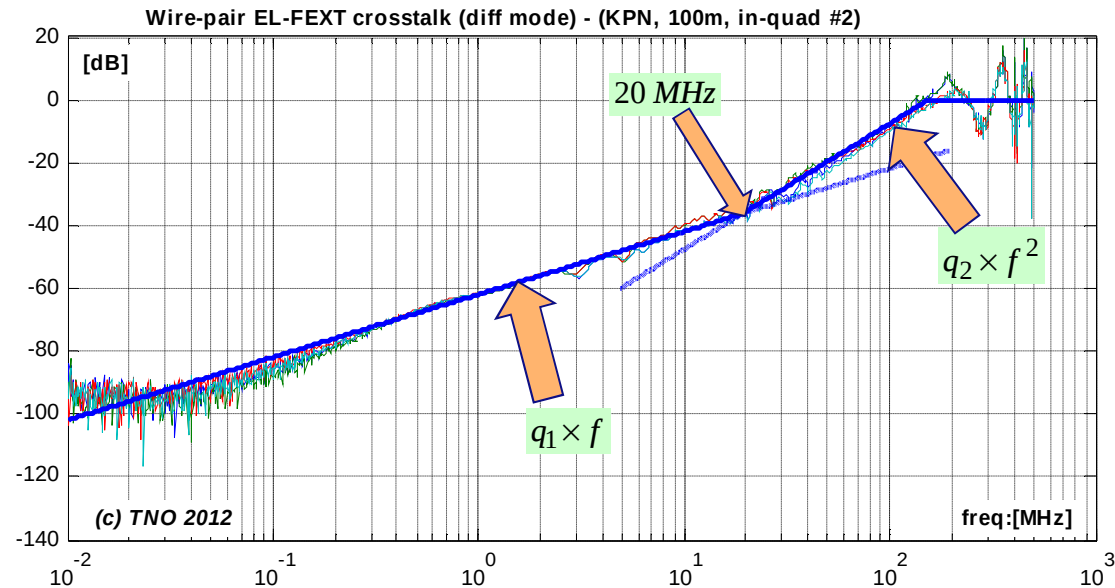
**Performance studies for
G.fast will be too optimistic
when this is ignored**

3. Progress on crosstalk modeling - EL-FEXT with dual slope

KPN Access cable,
100m, in-quad,
group 2



104m

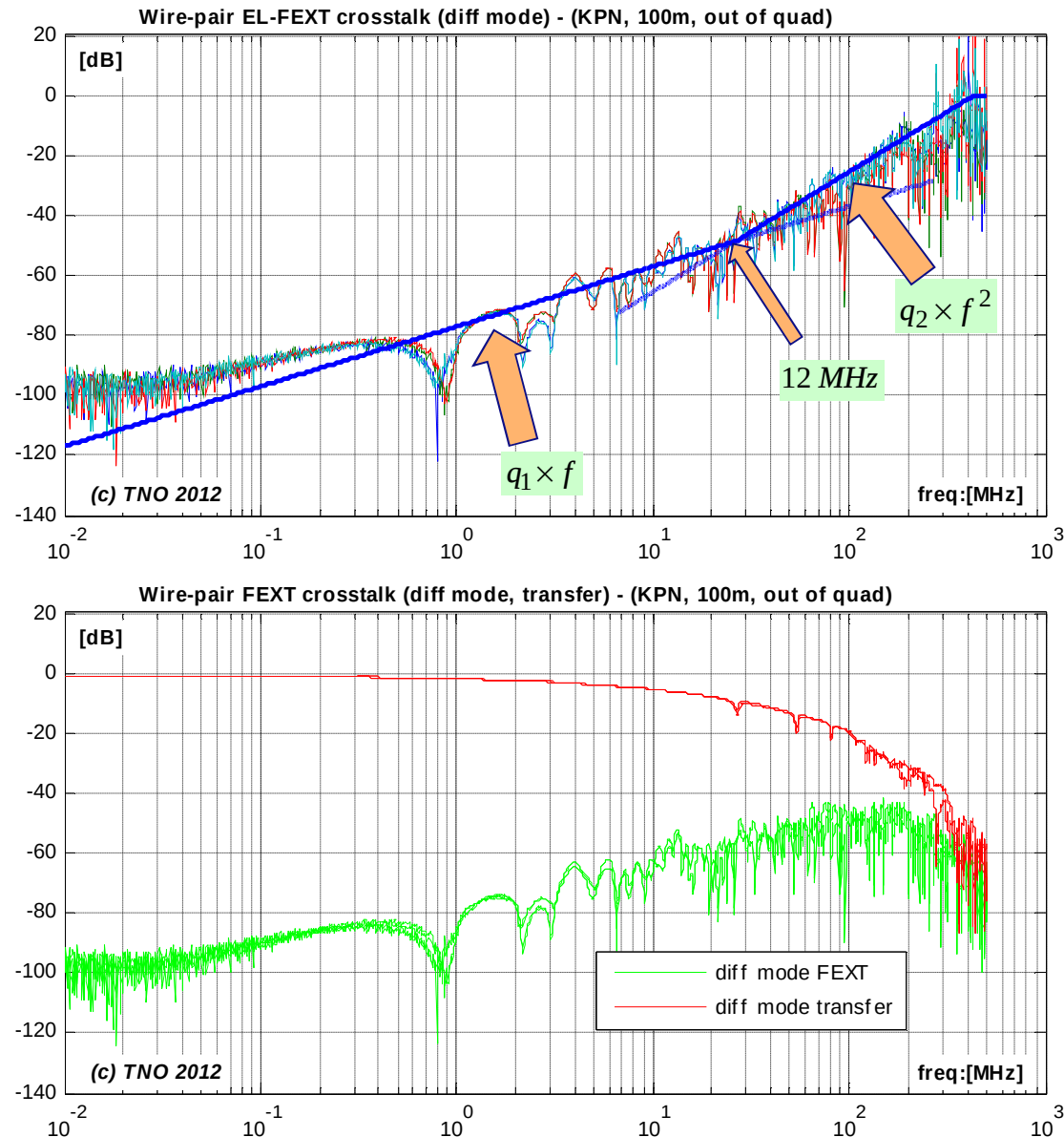


3. Progress on crosstalk modeling - EL-FEXT with dual slope

**KPN Access cable,
100m, out-of-quad**



104m



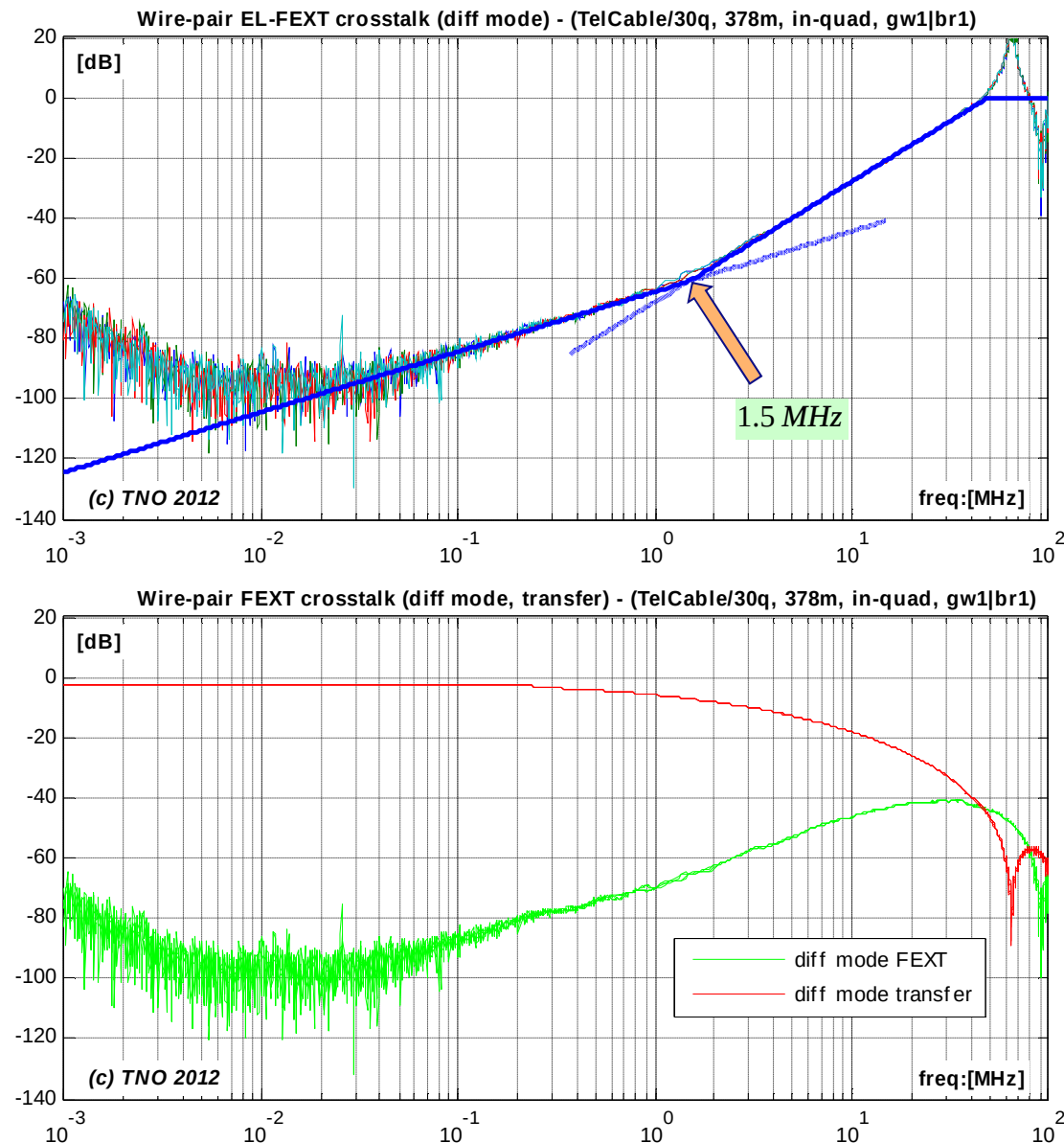
3. Progress on crosstalk modeling - EL-FEXT with dual slope

**Multi quad
telephony cabling,
378m, in-quad,
group 1**



378 m

**This cannot be
ignored for even
VDSL frequencies!
(roughly 1.5 MHz)**



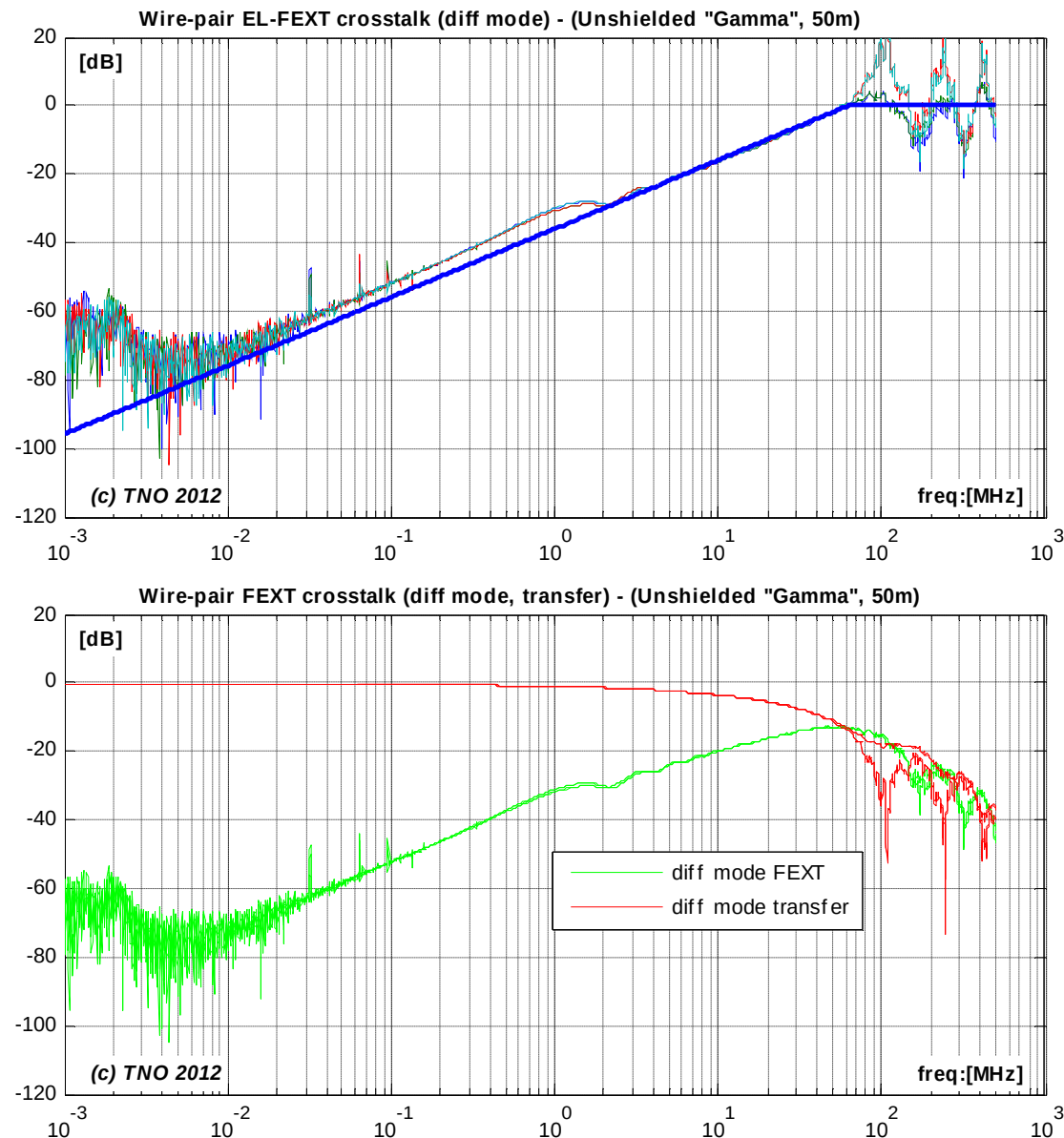
3. Progress on crosstalk modeling - EL-FEXT with dual slope

Low quality
telephony cable
found in consumer
shop (Gamma), 50m



51m

Crosstalk is soo
high, dual slope
effect not present



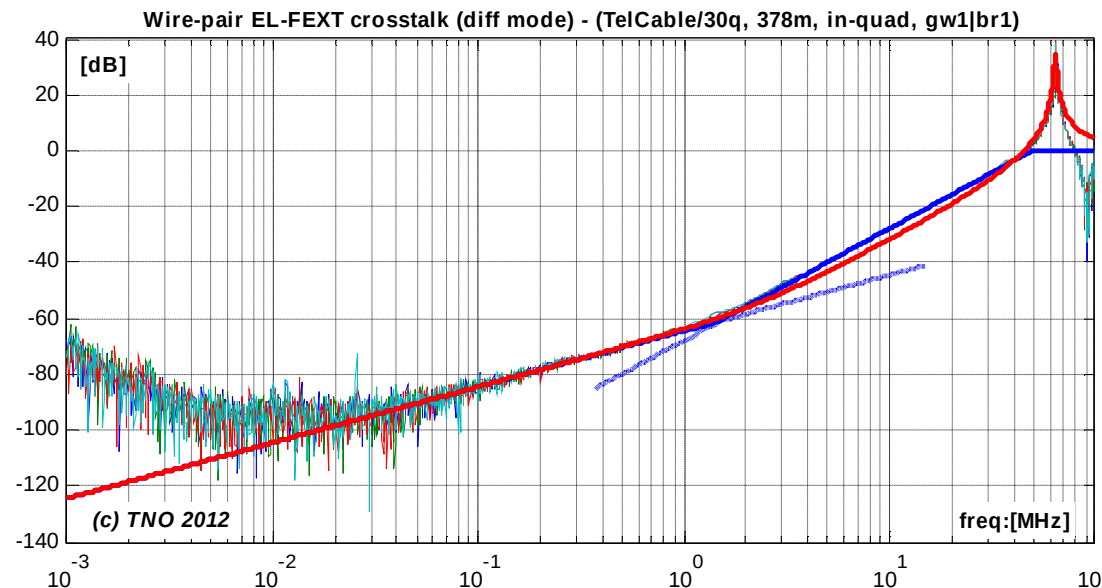
3. Progress on crosstalk modeling - EL-FEXT via 2nd-order transfer

How to model this?

à Dual slope = 2nd order transfer function

Models dual-slope
effect very well, ...

... models even the
resonance peak, ...

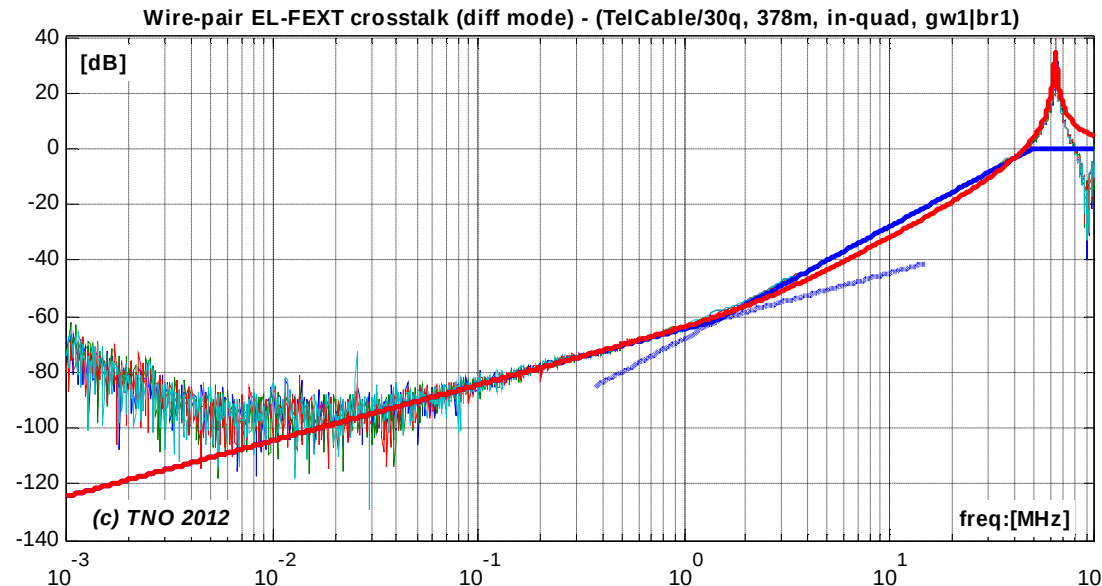


3. Progress on crosstalk modeling - EL-FEXT via 2nd-order transfer

$$H_{EL-FEXT}(j\omega) = \frac{\left(\frac{j\omega}{w_1} \right) \times \left(1 + \frac{j\omega \times w_1}{w_2 \cdot w_2} \right)}{1 + 2/q \cdot \left(\frac{j\omega}{w_2} \right) + \left(\frac{j\omega}{w_2} \right)^2}$$

Models dual-slope
effect very well, ...

... models even the
resonance peak, ...

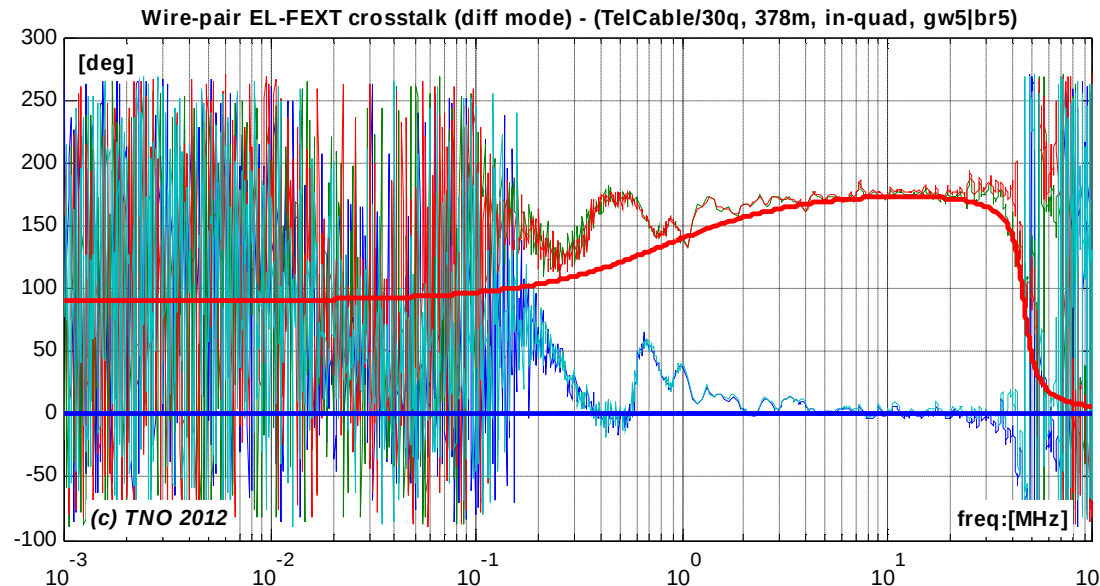


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Models dual-slope
effect sometimes
very well, ...

... and also the phase
(in quad cables)



3. Progress on crosstalk modeling - EL-FEXT via 2nd-order transfer

New approach

is gaining acceptance in ITU

4. Progress on performance studies – approach

**GOAL: Predict attainable bitrates
within a given scenario**
(Important in system design phase)

Traditional approach: Frequency domain calculations

› How:

- Calculate SNR from cable models and noise assumptions
(*from frequency domain calculations*)
- Run bit loading algorithm with the SNR
- Remove overhead of Cyclic Extension (prefix + suffix) and coding.

› Advantages

- Simple
- Adequate for channels dominated with additive white Gaussian noise (AWGN)

4. Progress on performance studies – approach

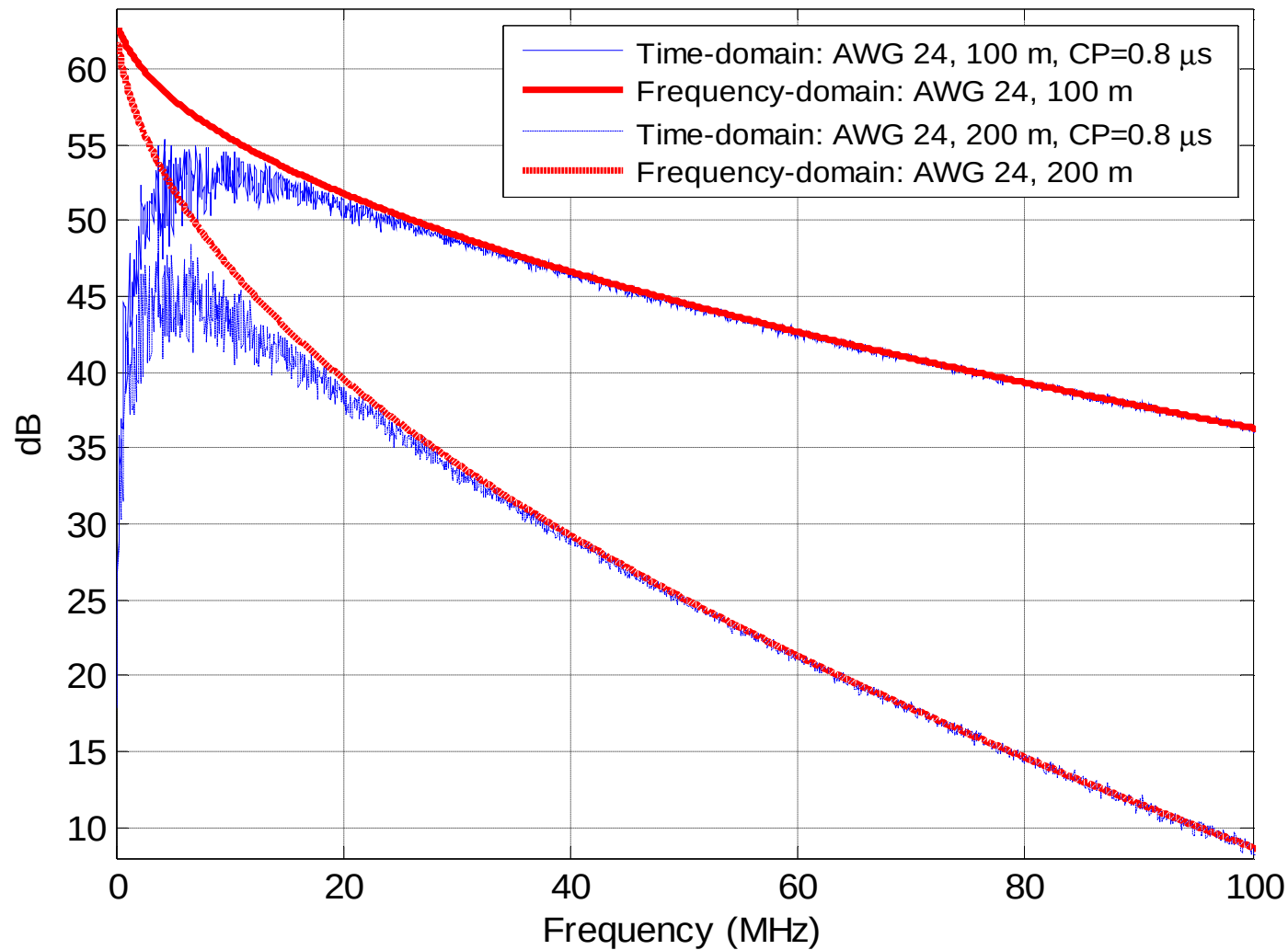
GOAL: Predict attainable bitrates within a given scenario
(Important in system design phase)

Advanced approach: Time domain calculations

- › **Why:** G.fast channel can be more ISI limited, especially with short cyclic prefix,
 - High tone spacing -> short symbol period
 - Long dispersion due to bridge taps
 - CP may not cover the whole channel dispersion.
- › **How:** Take inter-symbol interference (ISI) into consideration for estimating Signal to Noise and Interference Ratio estimation (SINR)
 - Calculate that via impulse response of (improved) cable model
 - Estimate SINR from a time domain simulation from training symbols
Implementation of symbol timing detection (or frame detection) and Frequency domain equalizer (FEQ) are needed.
 - Upsampling is needed to reduce windowing effects of Inverse Discrete Fourier Transform (IDFT) when generating impulse noise

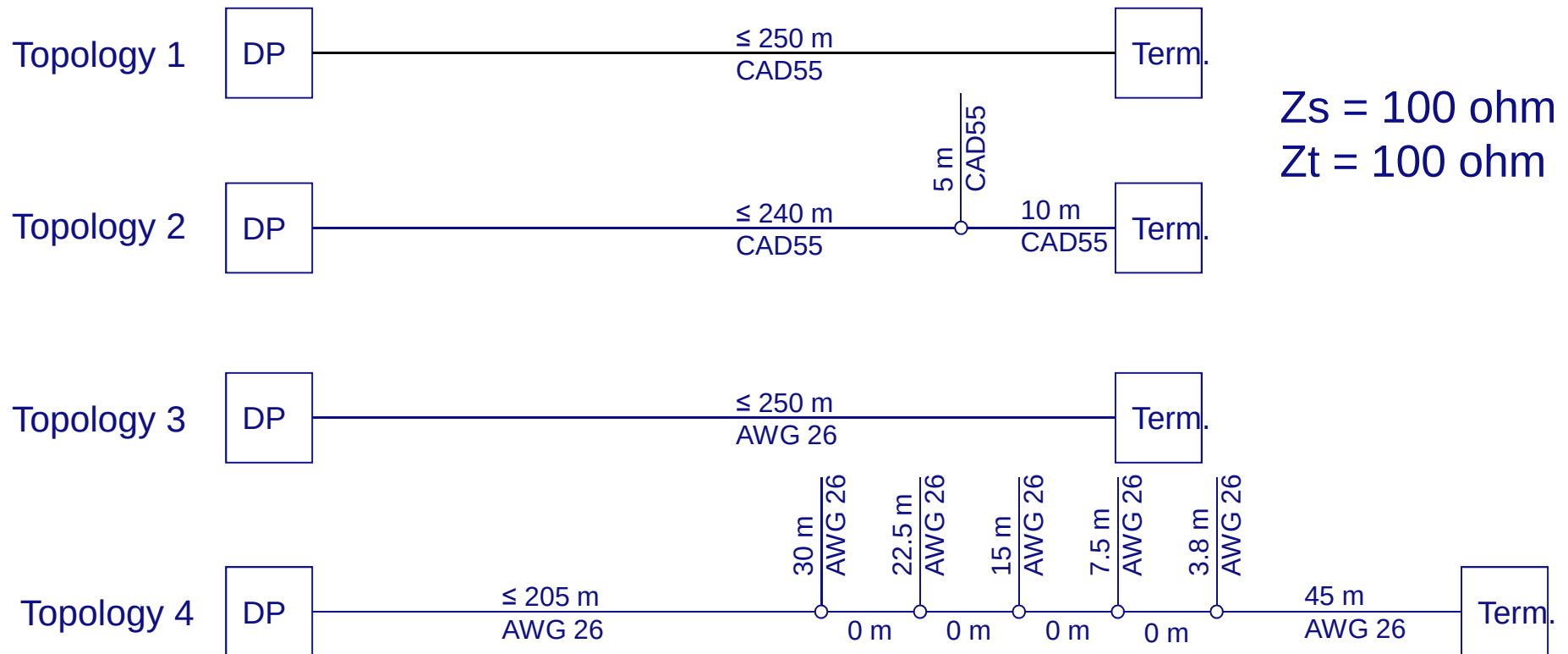
4. Progress on performance studies – approach

SNR comparison: time vs. frequency domain approach



4. Progress on performance studies – initial studies

Initial studies: **Selected loop topologies**



References:

- Loop topology: “G.fast: Wiring topologies and reference loops”, (ITU 11GS3-100)
- CAD55 model: BT, “G.Fast: Cable Models ”, (ITU 11RV-026)
- AWG 26 model: ANSI TP1 (ANSI T1.417-2003)

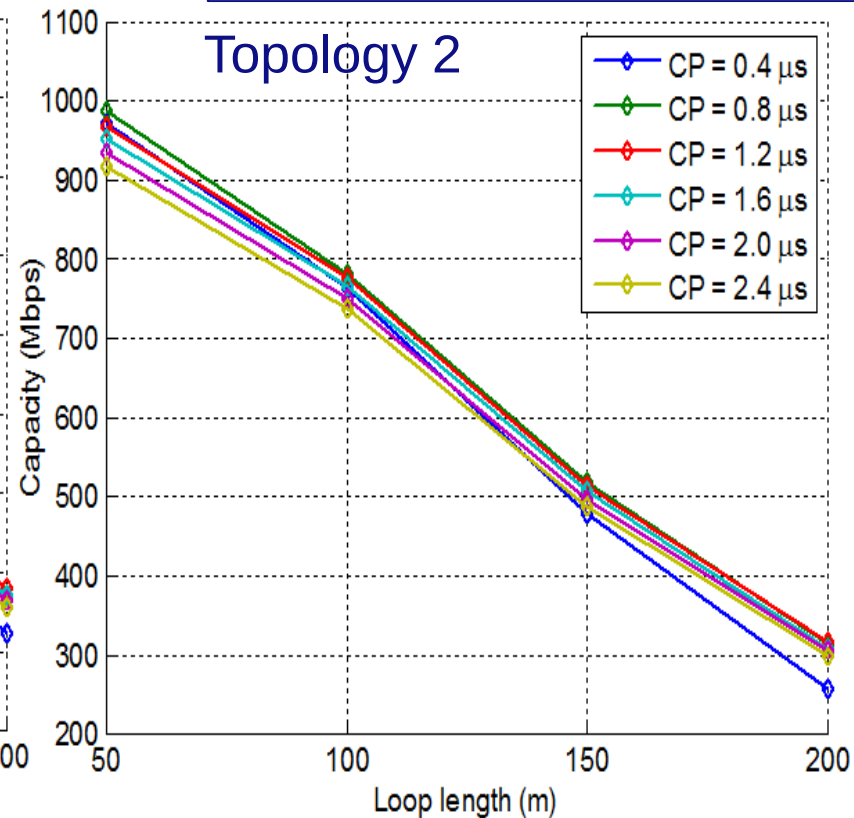
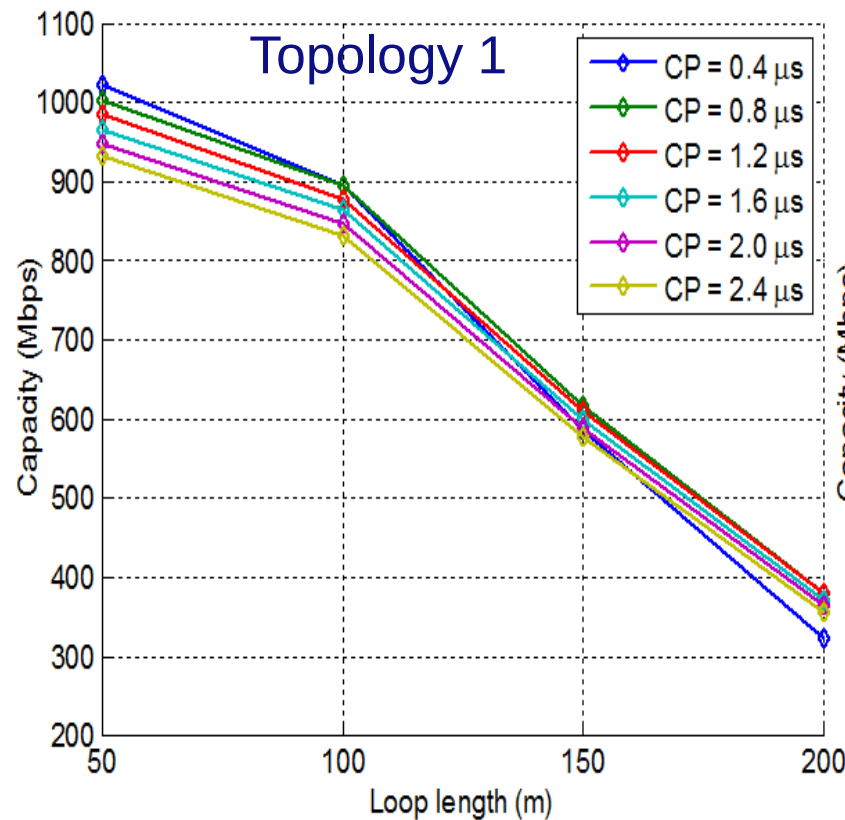
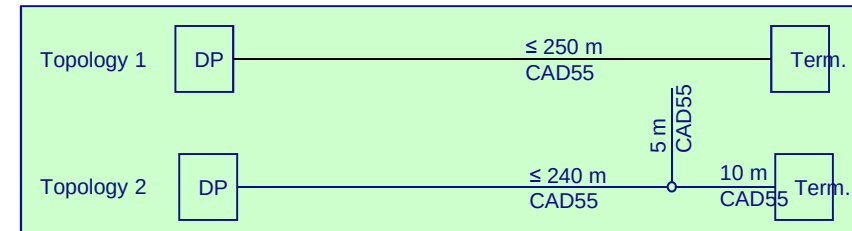
4. Progress on performance studies – initial studies

Initial studies: Simulation assumptions

- Channel bandwidth: 200 MHz
 - Channel is filtered with 53-tap FIR filter to reduce ringing from windowing effects of IDFT.
- Tone spacing: 48.84 KHz
- Data Bandwidth: 3.5 - 100 MHz
- Number of tones: 2048
 - Tone 0 is DC. Tones below 3.5 MHz are not loaded.
 - FFT size: 8192. FFT oversampling is used for fitting channel bandwidth.
- Signal PSD: -76 dBm/Hz
- AWGN noise: -140 dBm/Hz
- Coding: RS + Trellis
 - RS: $N/R = 255/16$.
 - Trellis: 0.5 bit/tone overhead.
 - Total coding gain = 5 dB.
- SNR gap: 9.75 dB
- SNR margin: 6 dB
- Bit loading: 1-12 bits
- Cyclic Extension: 0.4 μ s, 0.8 μ s, 1.2 μ s, 1.6 μ s, 2.0 μ s, 2.4 μ s
(Prefix+Suffix)
- Loop length (DP to terminal): 50 m, 100 m, 150 m, 200 m

4. Progress on performance studies – initial studies

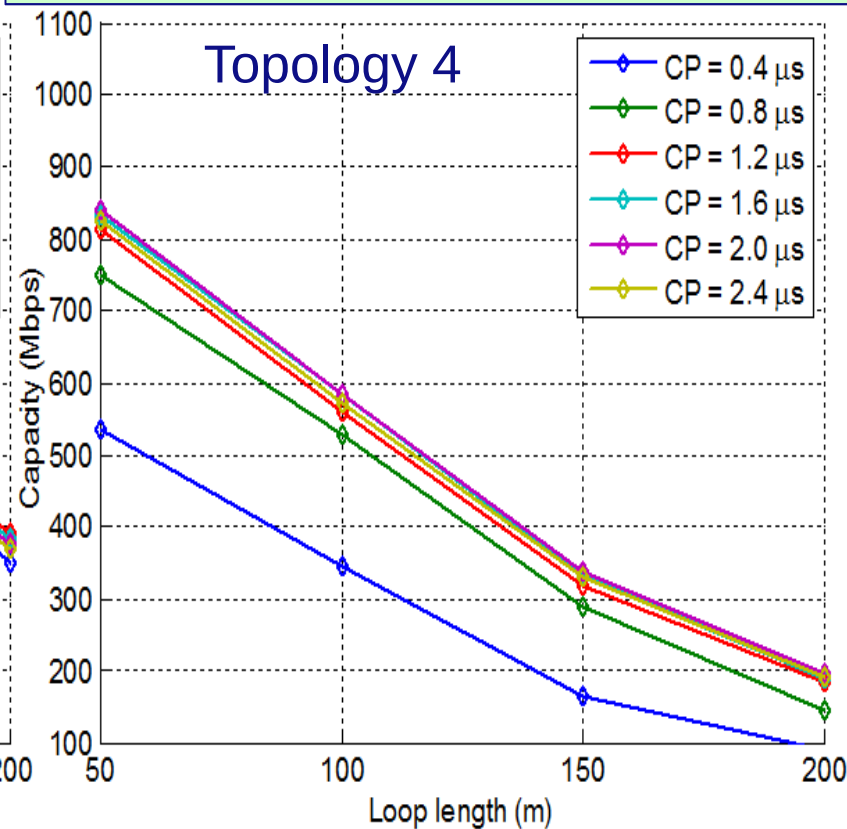
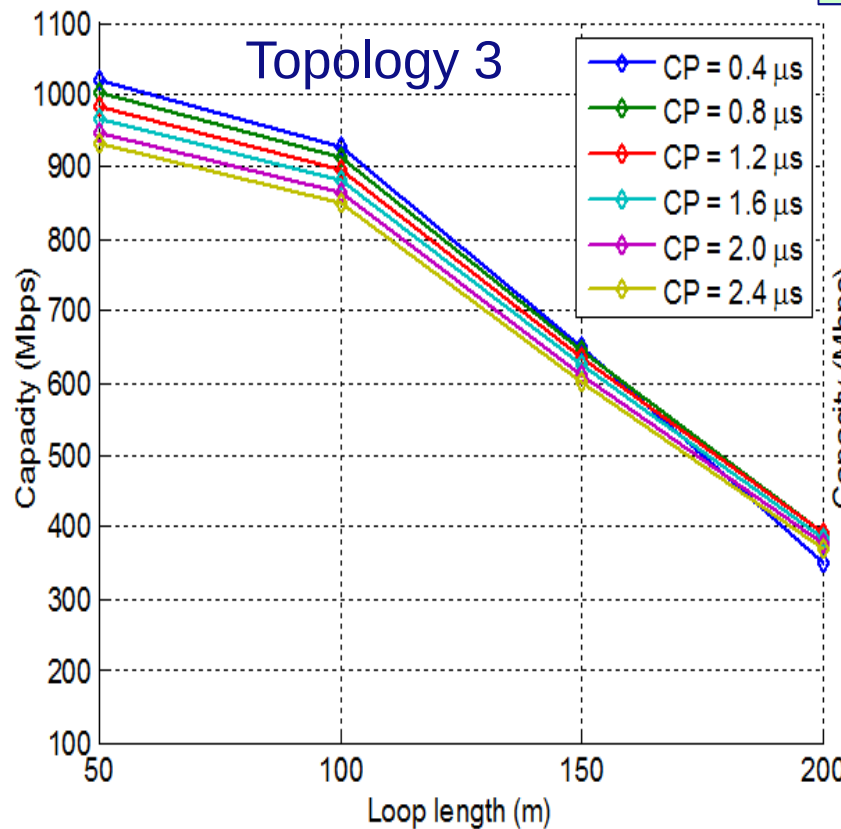
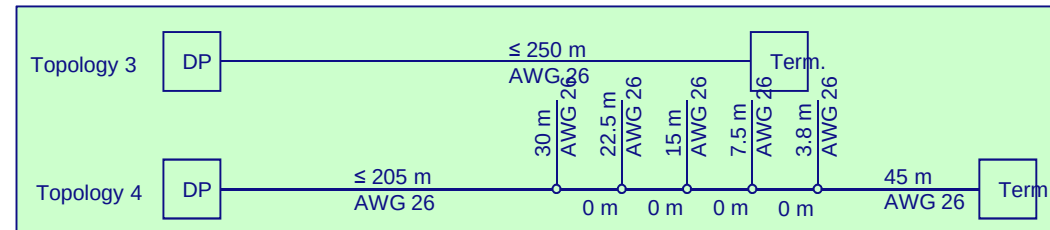
Initial studies: Bitrate results



- Topology 1&2: Optimal CP = 0.8 μ s, CP overhead = 3.76%
- Up to about 100 Mbps decrease due to a 5-meter bridge tap.

4. Progress on performance studies – initial studies

Initial studies: Bitrate results



- Topology 3: optimal CP = 0.4 or 0.8 μ s, CP overhead = 1.88% or 3.76%.
- Topology 4: optimal CP = 2 μ s, CP overhead = 8.9%.
- More than 300 Mbps rate loss can be seen due to multiple bridge taps of star topology.

5. Conclusions

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G.fast standardization is progressing very well

- Concept of Hybrid FttH via G.fast Initiated by 4GBB consortium
- global industry is now active in ITU to develop G.fast
- Aimed ITU deadline (dec 2012: consent on G.fast) is just a first phase

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**Cable models have been developed for hundreds of MHz,
so use them to describe your cable plant**

